



# IYPT — AUSTRALIA

## QUESTION 17: CRAZY SUITCASE

Reporter: Jeong Han Song

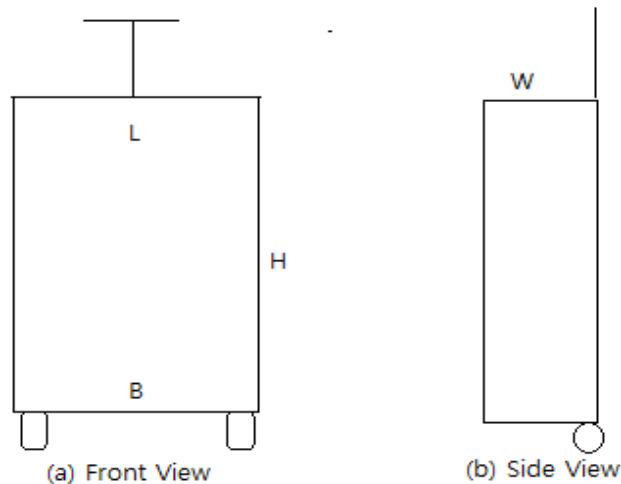
# PROBLEM

When one pulls along a **two wheeled suitcase**, it can under certain circumstances **wobble so strongly** from side to side that it can **turn over**. Investigate this phenomenon. Can one **suppress** or **intensify** the effect by **varied packing** of the luggage?



# TERMS & DEFINITIONS

When one pulls along a two wheeled suitcase, it can under certain circumstances wobble so strongly from **side to side** that it can turn over. Investigate this phenomenon. Can one suppress or intensify the effect by varied packing of the luggage?



$L = \text{length} = 40 \text{ cm}$

$H = \text{height} = 50 \text{ cm}$

$B = \text{distance between two wheels} = 39 \text{ cm}$

$W = \text{width} = 20 \text{ cm}$

$$\tau = Fd$$

Detachment of both wheels

Different Positions of Centre of mass

# FLOW CHART

## Qualitative Analysis

- Stages of motion of the wobbling suitcase
- Condition of overturn



## Quantitative Analysis

- Net Torque Equation
- Human Effect (Literature Review)
- Graphical Simulation (Theoretical Prediction)



## Experiment

- Measurement of angular displacement
- Computational Analysis
- Angular Acceleration (Derivation of force)



## Additional circumstances

- Walking frequency
- Coefficient of Restitution
- Different mass density
- Angle of tilt



**Relevant Condition for Overturn**



# QUALITATIVE ANALYSIS

- Cases for different effective height
- Five different phases

# STAGE 1: INITIAL CONDITION

Titled

Net Force = 0

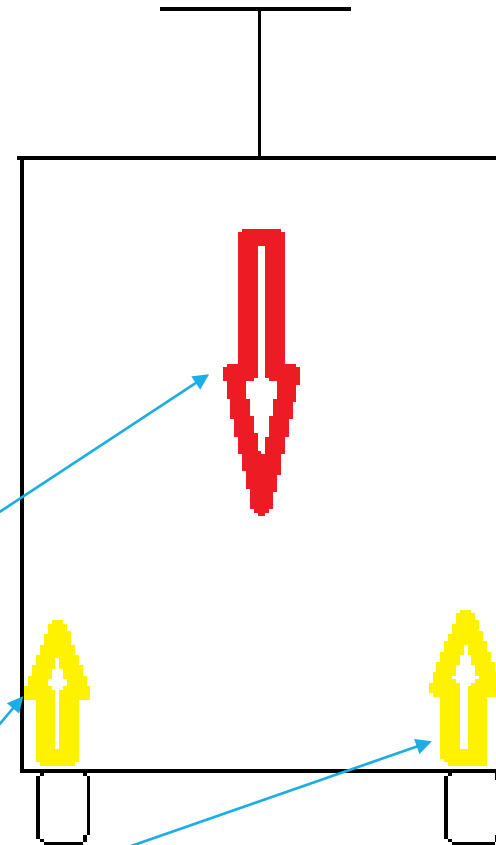
No External Force

Acceleration = 0 (i.e. Constant Speed)

Both wheels are in contact with the floor

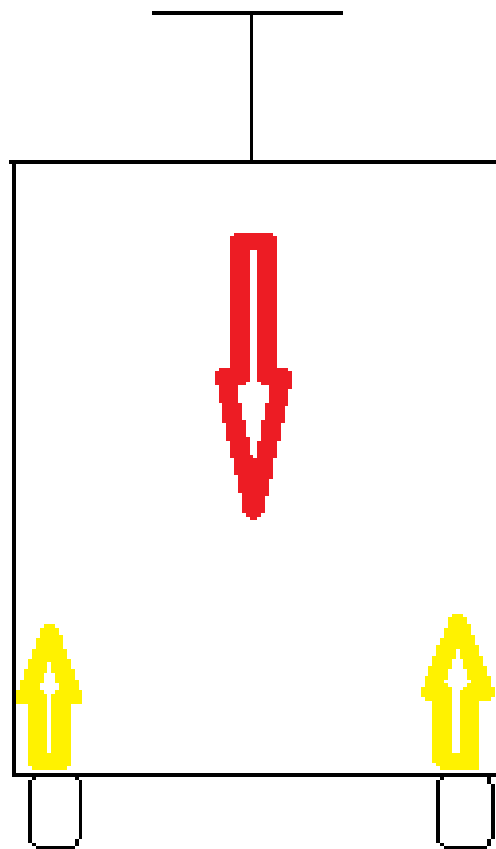
Weight of a suitcase

Normal Force by two wheels



(a) Front View

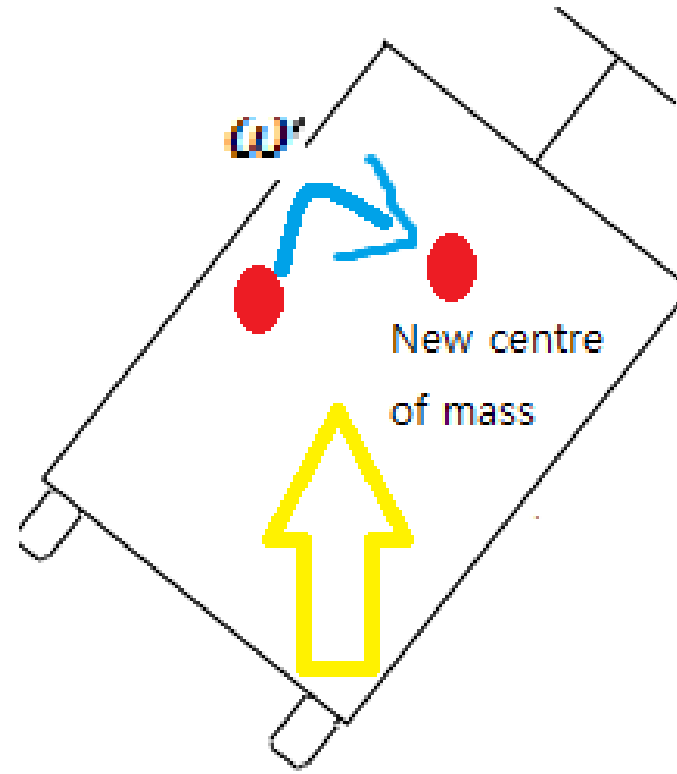
## STAGE 2: EFFECT OF INITIAL DISTURBANCE



(a) Front View



BUMP



(a) Front View

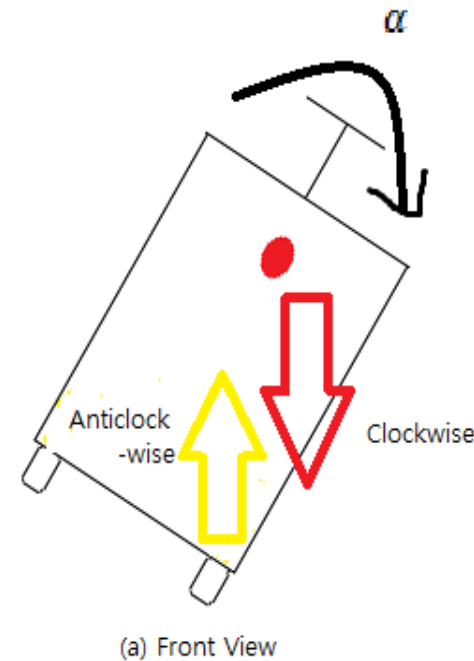
# STAGE 2:

## EFFECT OF INITIAL DISTURBANCE (TORQUE)

- Different effect depending on the position of weight

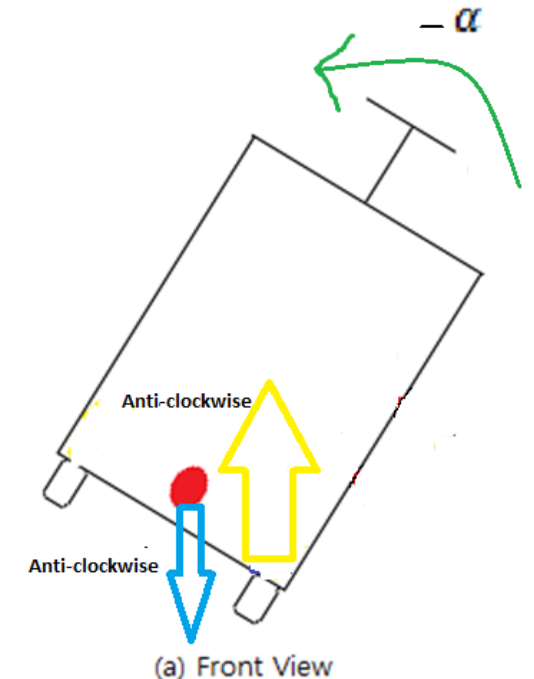
- **Case 1: High weight**

- Centre of mass now causes rotation about the supporting wheel
- Torque created by the center of mass
- Angular acceleration is present



- **Case 2: Low weight**

- Low centre of mass acts as a restoring force that opposes the original torque created by the initial disturbance
- Diminishes the wobble effect



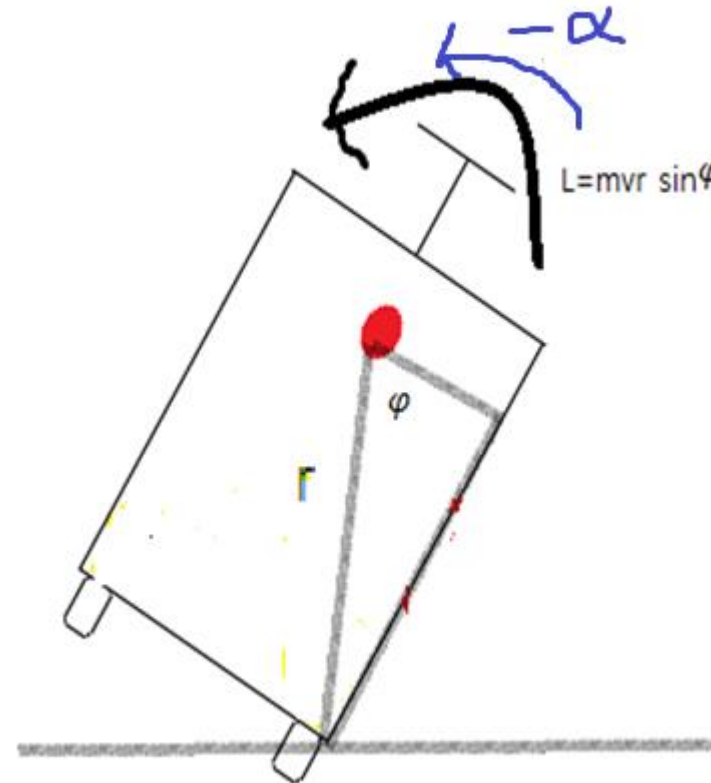


# STAGE 3: HUMAN RESPONSE

Human exerts a **periodic force** that **opposes** the disturbance created by the weight.

**Opposite direction** to the torque created by the weight

Effect of **inertia**

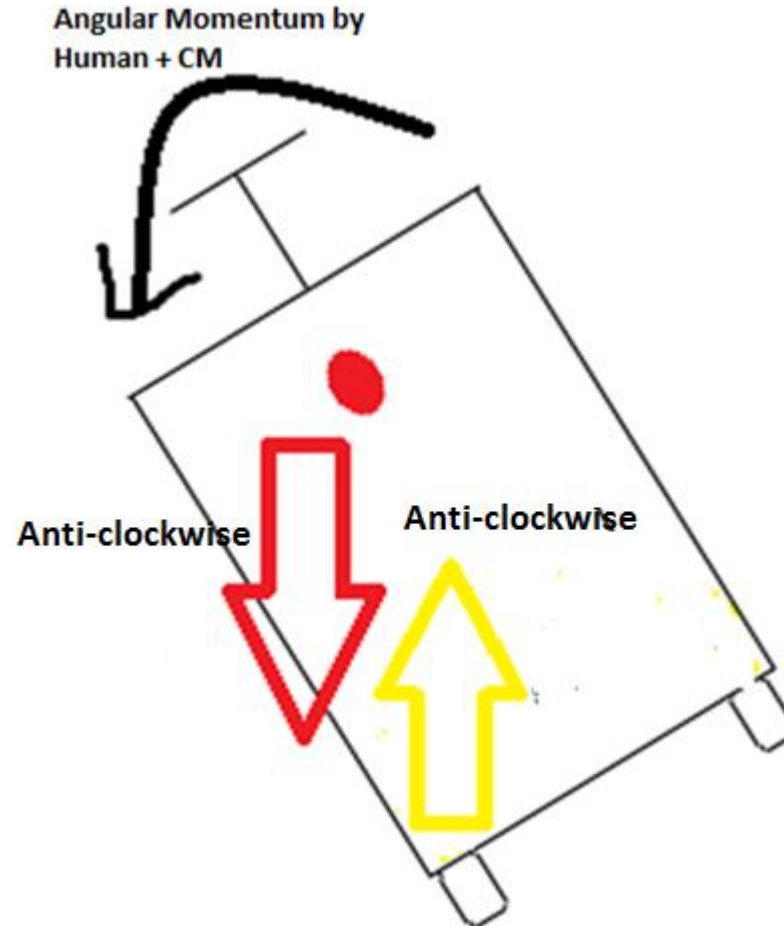


(a) Front View

# STAGE 4: POINT OF INSTABILITY

The **restoring force overshoots**

Overcompensation of restoring force would lead to the rather sharp increase in the oscillation.

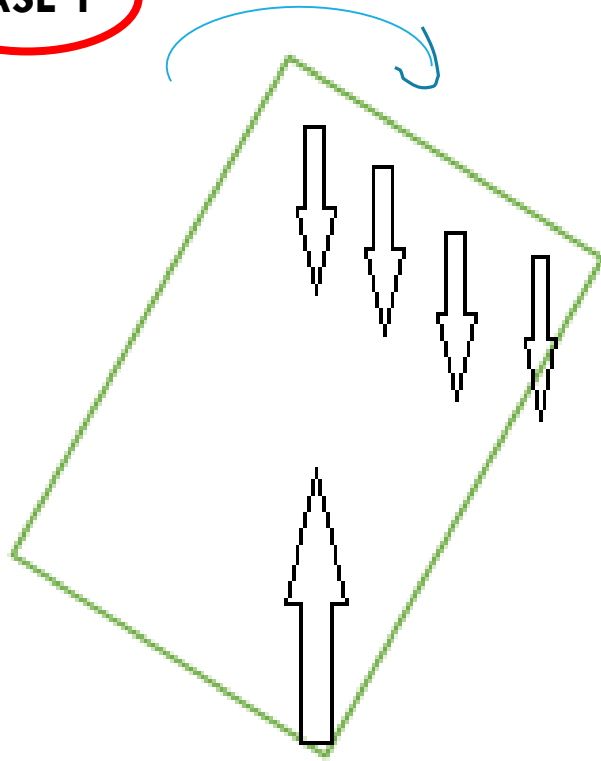


# STAGE 5: REPETITION AND AMPLIFICATION

When a suitcase meets a **critical amplitude** that exceeds what human can counteract, it **overturns**.

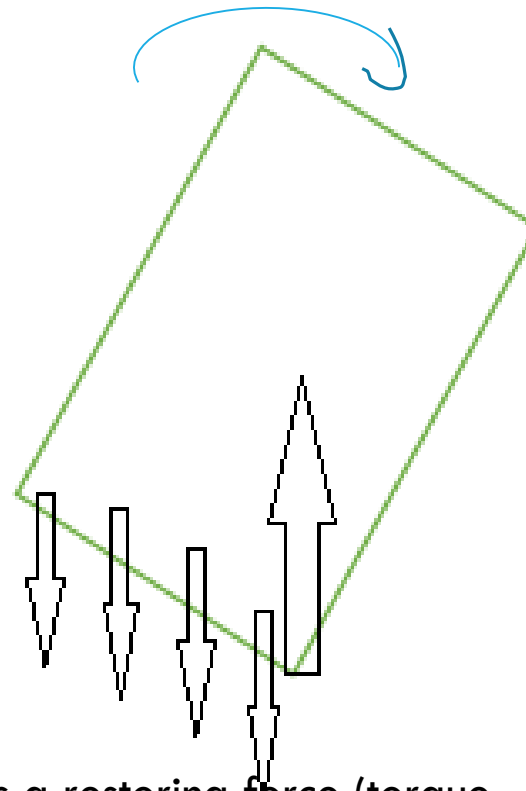
# QUALITATIVE MODEL – SUMMARY

**CASE 1**



Intensifies the initial disturbance  
(torque is applied in the same  
direction as disturbance)

**CASE 2**



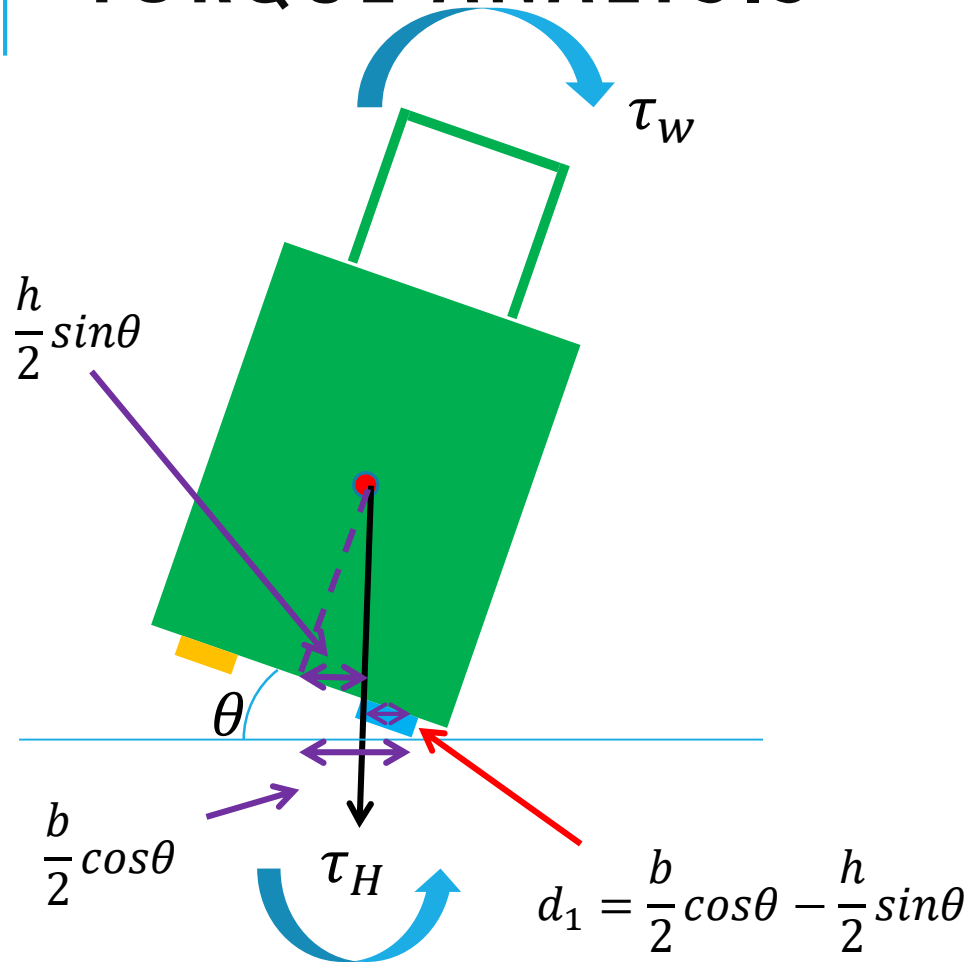
Acts as a restoring force (torque  
is applied in the opposite  
direction as disturbance)



# QUANTITATIVE ANALYSIS

- Net Torque Equation
- Literature Review: Suherman's model
- Theoretical Prediction (Graphical Simulation)

# TORQUE ANALYSIS



Two Types of torque:

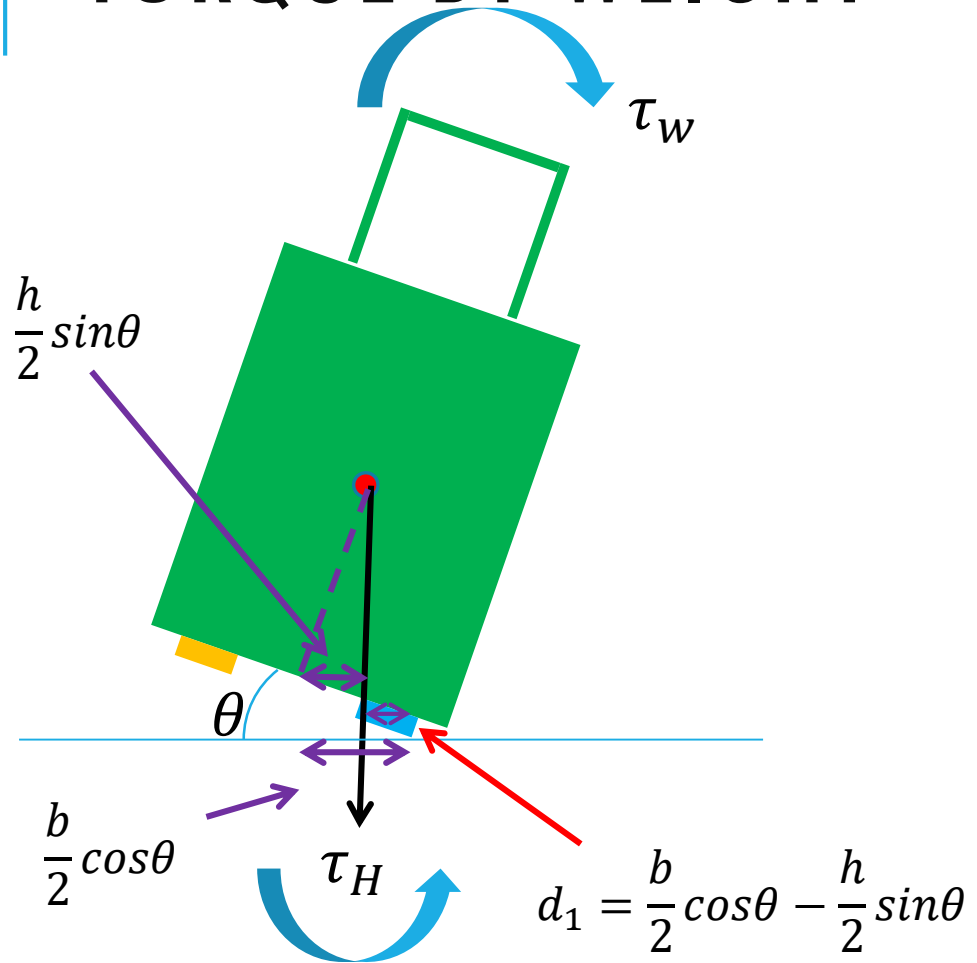
- 1) Torque by Weight
- 2) Torque by Human

Net Torque Equation:

$$I \frac{d\theta}{dt^2} = \tau_H - \tau_w$$

(Opposite Direction)

# TORQUE BY WEIGHT



From basic torque equation:

$$\tau = F \times d_1$$

Force is equivalent to the weight

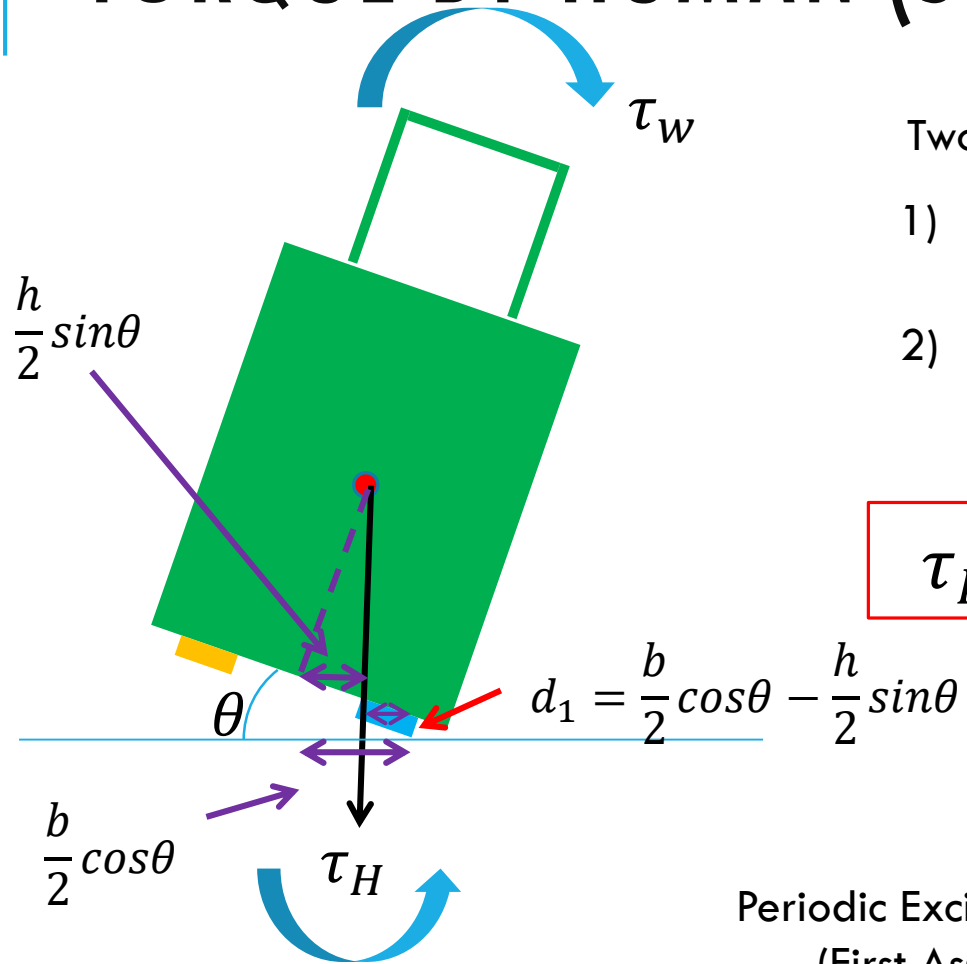
$$F = mg$$

Shortest distance is:

$$\Rightarrow \frac{b}{2} \cos \theta - \frac{h}{2} \sin \theta$$

$$\therefore \tau_w = mg \left( \frac{b}{2} \cos \theta - \frac{h}{2} \sin \theta \right) \dots (1)$$

# TORQUE BY HUMAN (SUHERMAN'S MODEL)



Two Fundamental Assumptions:

- 1) Puller's walking motion induces a periodic moment on the handle of suitcase
- 2) Puller exerts additional restoring moment to suppress the wobble proportional to rocking angle

$$\tau_H = q_\theta \sin(\omega t) - k\theta \quad \dots (2)$$

Periodic Excitation Torque  
(First Assumption)

Restoring Torque (Second  
Assumption)

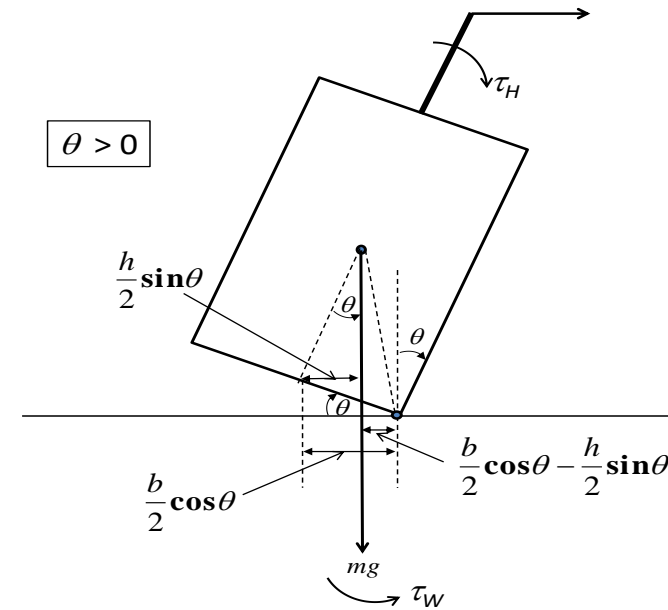
$\theta$ : angle of rocking  
 $q_\theta$ : amplitude of excitation torque  
 $\omega$ : walking frequency  
 $k$ : constant for restoring torque



# NET TORQUE EQUATION

Combining Equation 1 & 2:

$$I \frac{d^2\theta}{dt^2} = \tau_H - \tau_W$$



$$I \frac{d^2\theta}{dt^2} = q_0 \sin(\omega t) - k\theta - mg \left( \frac{b}{2} \cos \theta - \frac{h}{2} \sin \theta \right) \quad \dots \theta > 0$$

Or

$$I \frac{d^2\theta}{dt^2} = q_0 \sin(\omega t) - k\theta + mg \left( \frac{b}{2} \cos \theta + \frac{h}{2} \sin \theta \right) \quad \dots \theta < 0$$

# FINAL NET TORQUE EQUATION

Define:  $S = +1, \text{ if } \theta > 0$        $S = -1, \text{ if } \theta < 0$

→ SIMPLE

Final Equation:

→ ACCURATE

$$I \frac{d^2 \theta}{dt^2} = q_0 \sin(\omega t) - k\theta - Smg \frac{b}{2} \cos \theta + mg \frac{h}{2} \sin \theta$$

$b$ : bottom length of a suitcase

$h$ : effective height

$\theta$ : angle of rocking

$q_0$ : amplitude of excitation torque

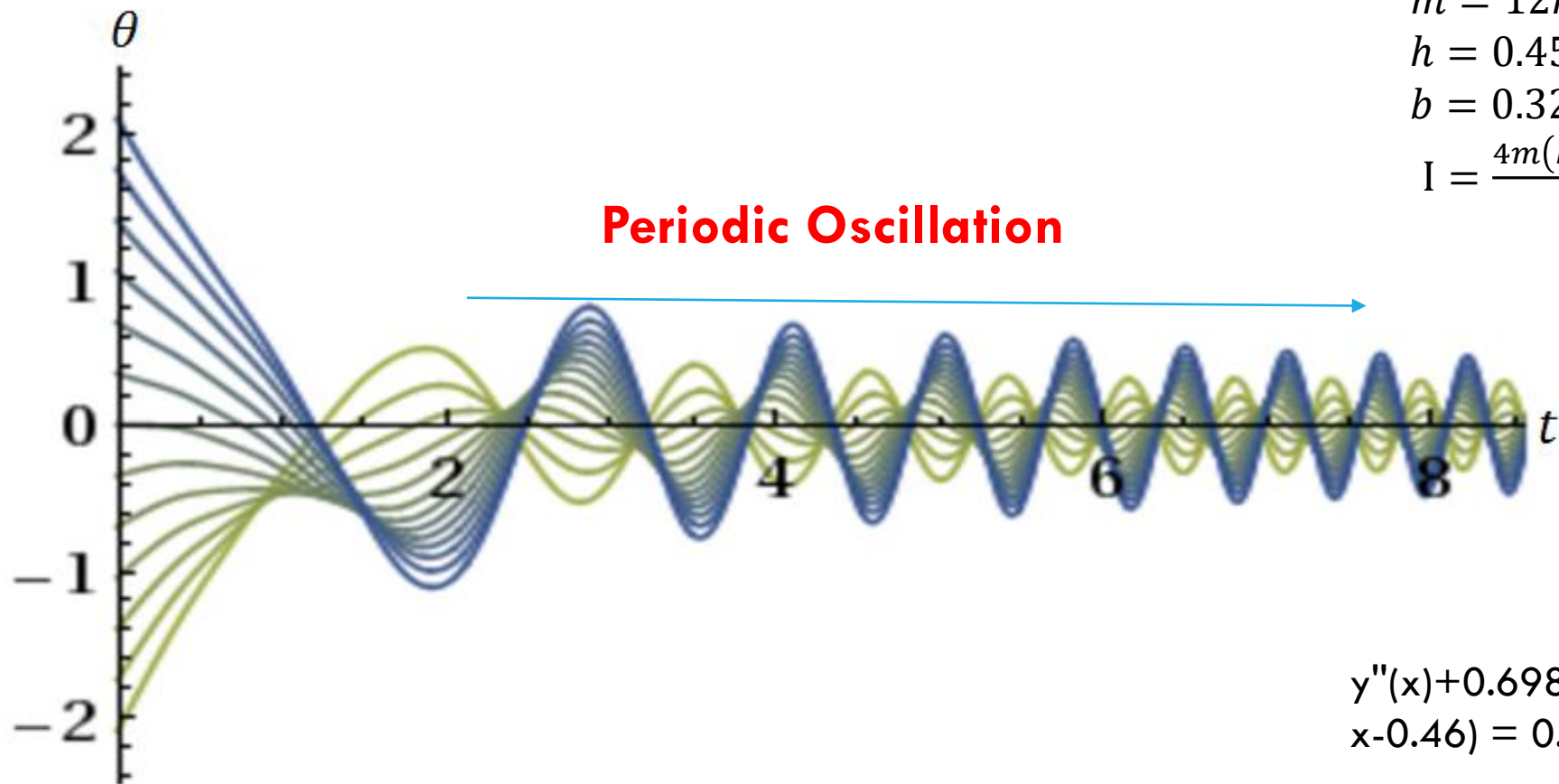
$\omega$ : walking frequency

$k$ : constant for restoring torque

As effective height increases, net torque increases!

# THEORETICAL PREDICTION – WOBBLE

Sample Graph from our computer simulation (wolfram alpha) using values below:



$$m = 12kg$$

$$h = 0.458m$$

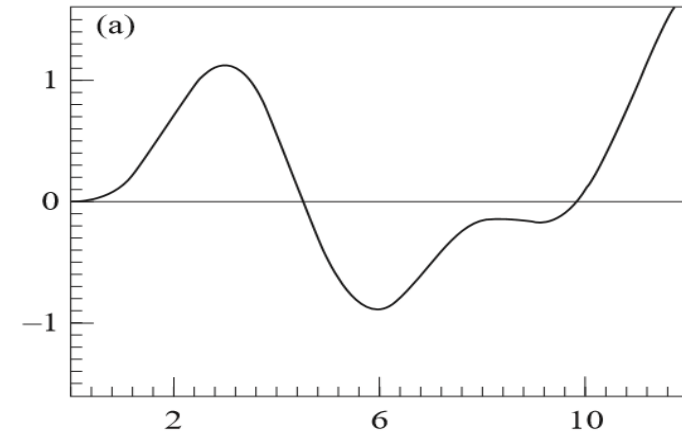
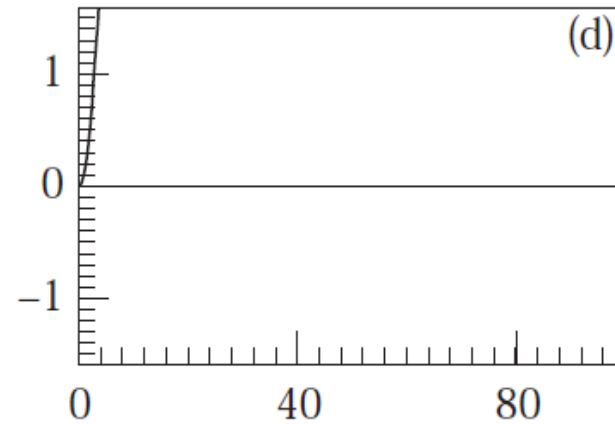
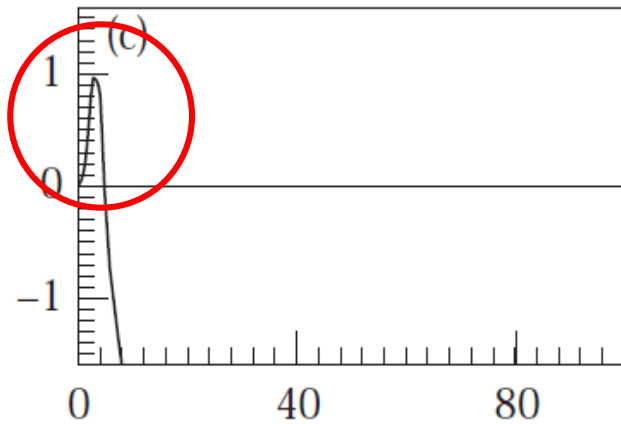
$$b = 0.320m$$

$$I = \frac{4m(h^2 + b^2)}{3} = 4.996 \text{ kgm}^2$$

$$y''(x) + 0.69869 \cos(y(x)) - \sin(y(x)) + y \times (2.3232x - 0.46) = 0.6 \sin(4.9946 \times 2.3232x + 0.426)$$

# LITERATURE REVIEW: SUHERMAN'S RESULTS

## OVERTURN OF A SUITCASE



1. Sharp change in angular displacement
2. No wobble during the overturn

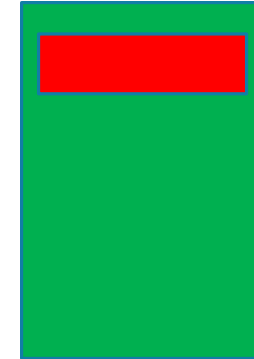
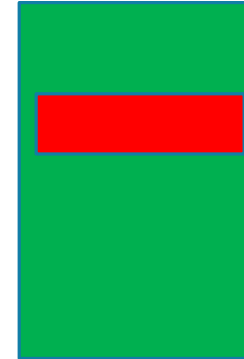
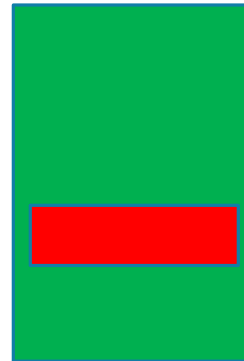
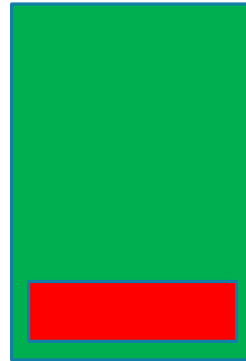
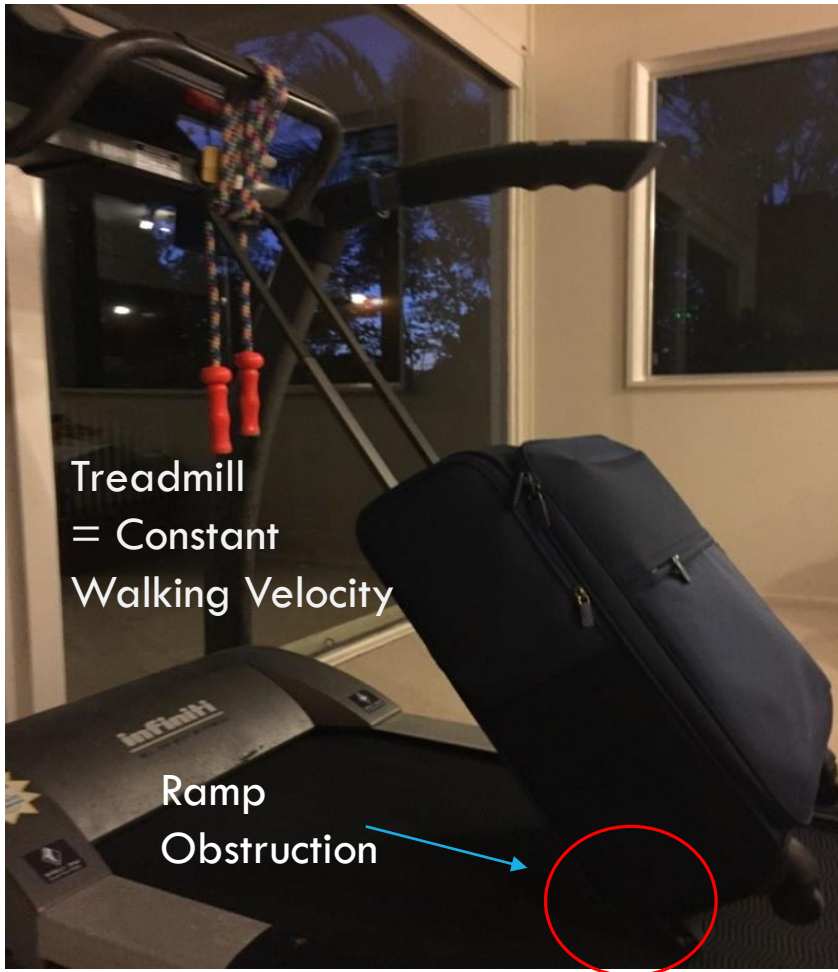
ROCKING ANGLE  $\nu$  TIME  
OVERTURN ( $\theta > \frac{\pi}{2}$ )



- Experimental Setup
- Angular displacement vs. time
- Computational Analysis

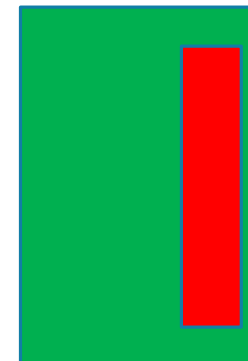
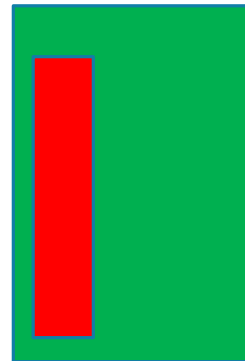
# EXPERIMENT

# EXPERIMENTAL SETUP



**SET A**

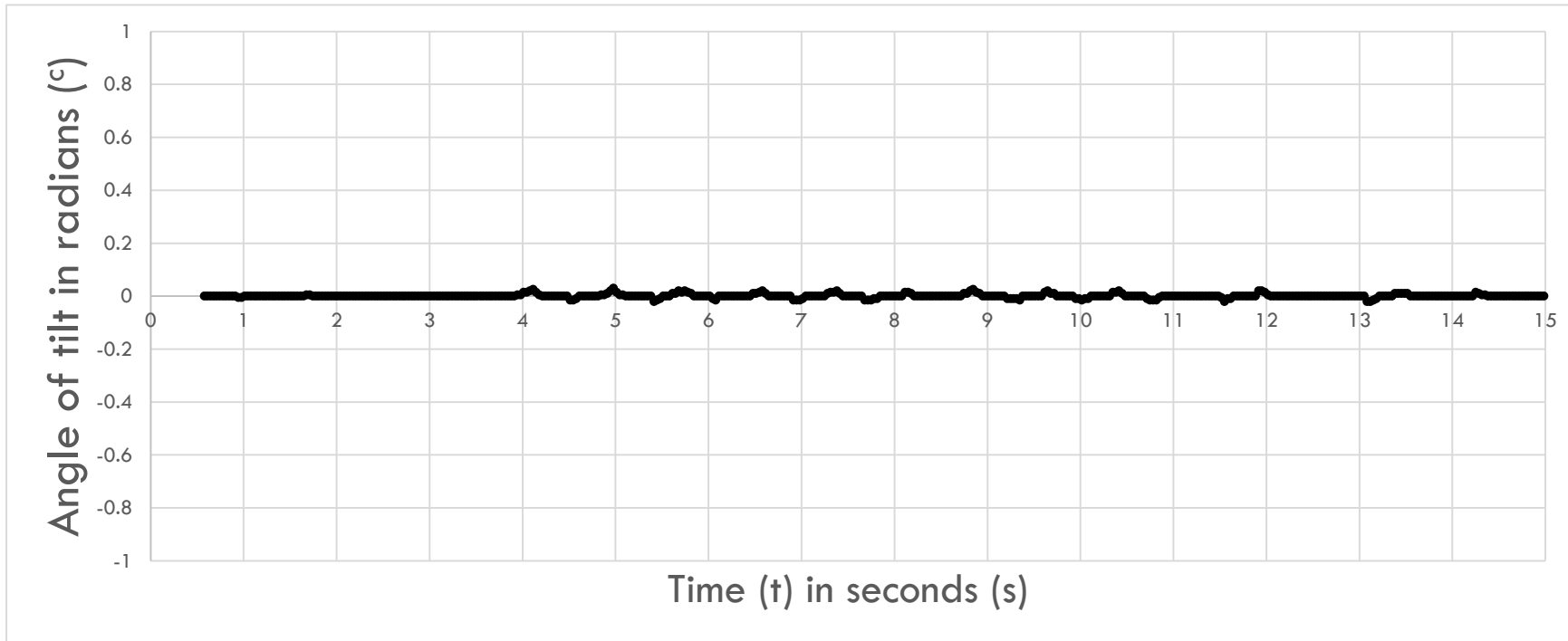
Height varied: 0.08m, 0.16m, 0.24m, 0.32m, 0.4m



**SET B**

Trackers Video Analysis

# RESULT 1: **0.08M** EFFECTIVE HEIGHT OF CM



- Very minimal angular displacement
- Inaccurate measurement (interval: 0.1 s)
- Hard to observe trend or data



**Fast Fourier Transform**

# SIMULATING THE EQUATION

In [2]: `import numpy`

```
data = numpy.genfromtxt(txt_file_name)
y_data = numpy.genfromtxt(txt_file_name, usecols=1)
Coef = numpy.fft.fft(y_data)
Freq = numpy.fft.fftfreq(len(y_data))
import matplotlib.pyplot as plt
Abs_Coef = numpy.abs(Coef)
%matplotlib inline
#plt.plot(Freq[:int(len(Freq)/2)], Abs_Coef[:int(len(Freq)/2)])
Pop_Coef = Coef[:equation_length]
Pop_Freq = Freq[:equation_length]
def graph(formula, x_range):
    x = numpy.array(x_range)
    y = eval(formula)
    plt.plot(x, y)
    plt.show()

Pop_Freq_complex = Pop_Freq.view(dtype=numpy.complex128)

equation = str(0)
for i in range(0, len(Pop_Coef)):
    equation = equation + '+' + str(Pop_Coef[i]) + '*numpy.exp(' + str(Pop_Freq[i]) + 'j*x)'

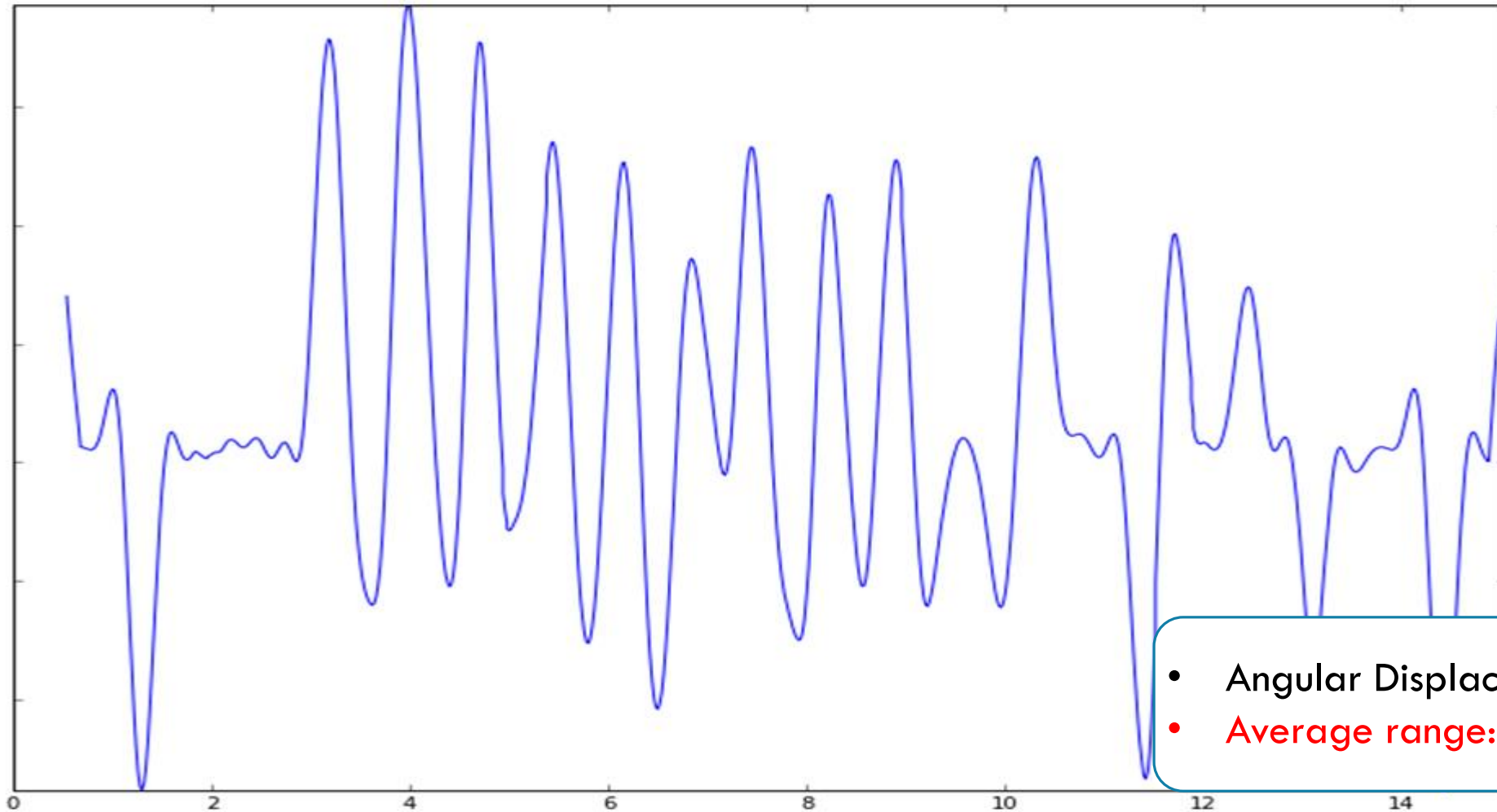
#graph(equation, range(0, graph_length))
print('')
print('The equation of the original graph:')
print('')
print(equation)
```

The equation of the original graph:

```
0+(1.67571644042+0j)*numpy.exp(0.0j*x)+(-0.39338130797-0.228859443672j)*numpy.exp(0.00135869565217j*x)+(-0.2407771180
86+0.294098934776j)*numpy.exp(0.00271739130435j*x)+(0.160951518353+0.292344341302j)*numpy.exp(0.00407608695652j*x)+
(0.0793870251769-0.0343400073869j)*numpy.exp(0.0054347826087j*x)+(0.128171884923+0.114165718316j)*numpy.exp(0.0067934
7826087j*x)+(-0.0789217710141+0.0506876519715j)*numpy.exp(0.00815217391304j*x)+(-0.313683719822+0.177882753422j)*numpy
y.exp(0.00951086956522j*x)+(-0.405657156874-0.341040410623j)*numpy.exp(0.0108695652174j*x)+(0.169831208229-0.27419970
4291j)*numpy.exp(0.012282608696j*x)+(-0.212322076372-0.0533675435594j)*numpy.exp(0.0135869565217j*x)+(-0.16271467461
5+0.0991007955451j)*numpy.exp(0.0149456521739j*x)+(-0.237838649698+0.49273818019j)*numpy.exp(0.0163043478261j*x)+(0.2
43829604558-0.0486385296346j)*numpy.exp(0.0176630434783j*x)+(-0.122470662683-0.0720897431264j)*numpy.exp(0.0190217391
304j*x)+(-0.353615922653-0.0570099119301j)*numpy.exp(0.0203804347826j*x)+(0.086710240439+0.322257867439j)*numpy.exp
(0.0217391304348j*x)+(0.369227221677-0.553337430946j)*numpy.exp(0.023097826087j*x)+(-0.690435890344-1.1958190939j)*nu
mpy.exp(0.0244565217391j*x)+(0.83962513333+0.98398930061j)*numpy.exp(0.0258152173913j*x)+(-0.374196414629-0.172350054
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22-0.0193382571159j)*numpy.exp(0.0326086956522j*x)+(0.179287240967+0.0884711698517j)*numpy.exp(0.0339673913043j*x)+
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xp(0.039402173913j*x)+(-0.365722068985+0.0285545452021j)*numpy.exp(0.0407608695652j*x)+(-0.470760261804-0.13846995373
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0.306363818756j)*numpy.exp(0.0448369565217j*x)+(0.111570601653-0.476449285374j)*numpy.exp(0.0461956521739j*x)+(-0.064
5311911822+0.151879156556j)*numpy.exp(0.0475543478261j*x)+(0.0789154712737+0.123058886322j)*numpy.exp(0.0489130434783
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6304347826j*x)+(-0.111432762432-0.196002257036j)*numpy.exp(0.0529891304348j*x)+(-0.186147288585+0.0571708417067j)*num
py.exp(0.054347826087j*x)+(-0.3143266197-0.105088205018j)*numpy.exp(0.0557065217391j*x)+(0.190001549056+0.11156075631
8j)*numpy.exp(0.0570652173913j*x)+(-0.138072497087+0.112684426125j)*numpy.exp(0.0584239130435j*x)+(-0.057339368746+0.
212359713763j)*numpy.exp(0.0597826086957j*x)+(-0.233019181104+0.341870946377j)*numpy.exp(0.0611413043478j*x)+(0.28190
923794-0.443785641915j)*numpy.exp(0.0625j*x)+(-0.0952119988175-0.0444826831503j)*numpy.exp(0.0638586956522j*x)+(-0.24
5611700998-0.0661981914326j)*numpy.exp(0.0652173913043j*x)+(0.175441186289+0.0283829135648j)*numpy.exp(0.066576086956
5j*x)
```

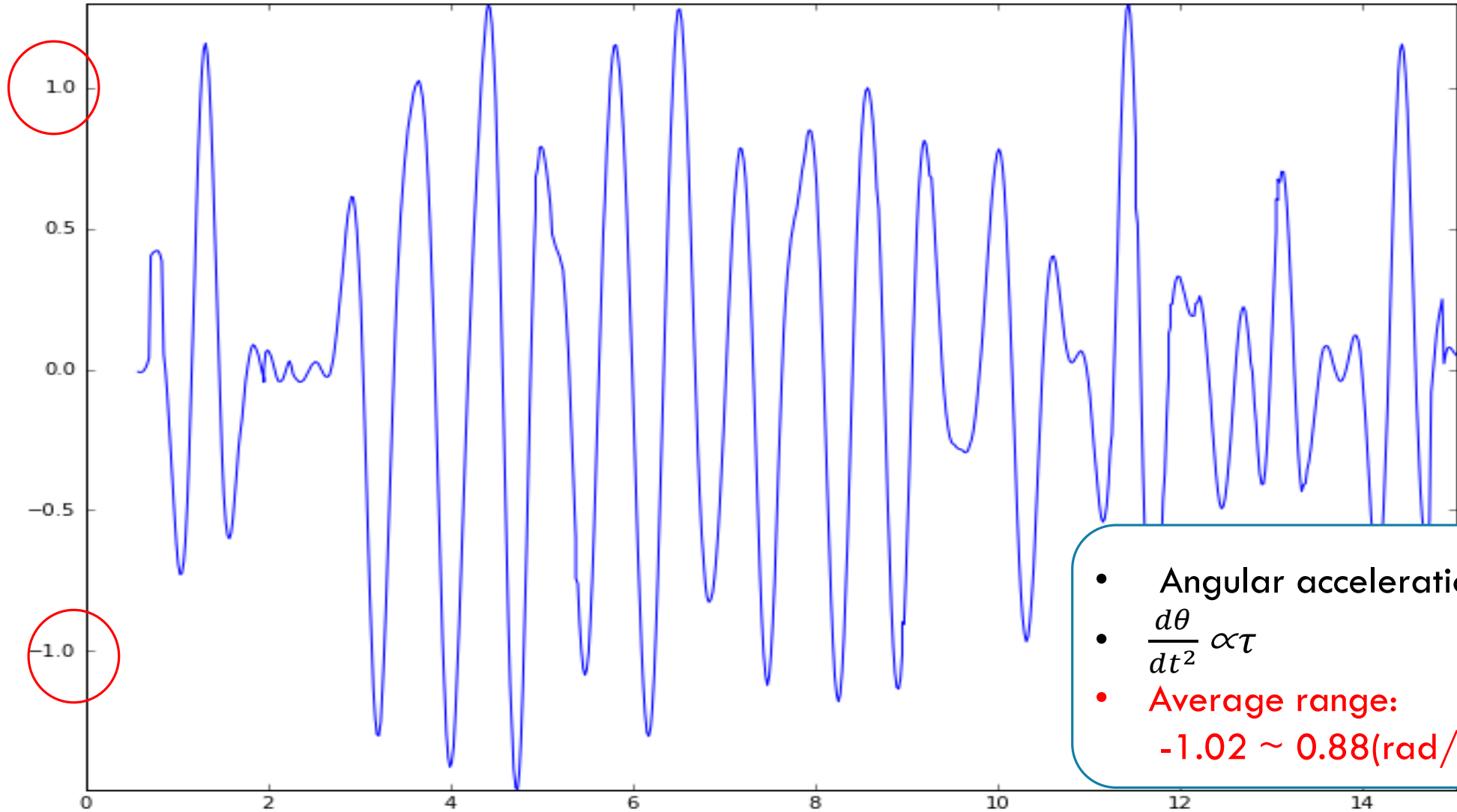


# ORIGINAL GRAPH (MAGNIFIED VERSION)



- Angular Displacement vs.Time
- Average range: -0.04 ~ 0.01 (rad)

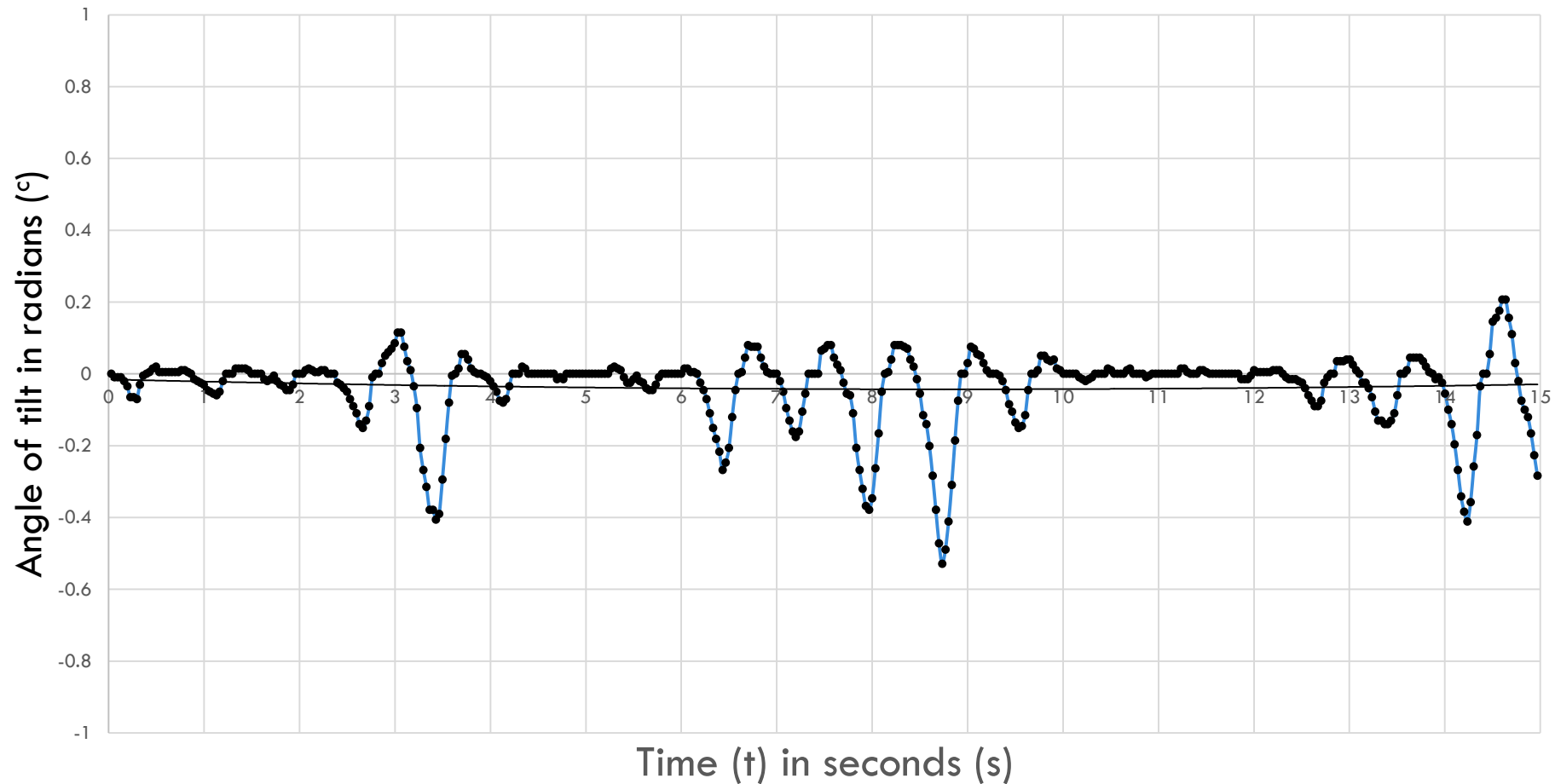
# SECOND DERIVATIVE (ANGULAR ACCELERATION)



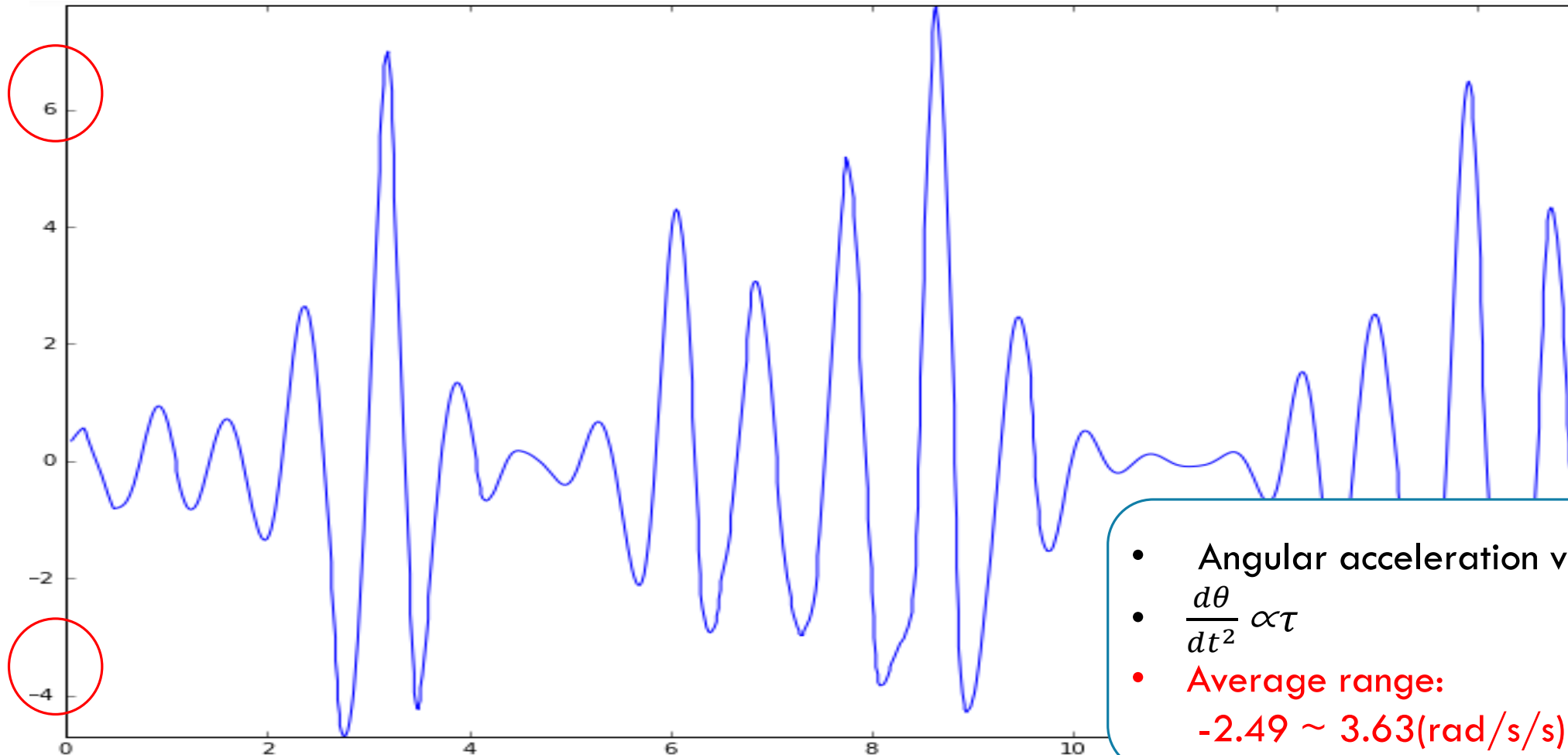
- Angular acceleration vs. time
- $\frac{d\theta}{dt^2} \propto \tau$
- Average range:  
-1.02 ~ 0.88(rad/s/s)

## RESULT 2: 0.16M EFFECTIVE HEIGHT OF CM

Angle of tilt of the centre of the suitcase from vertical ( $\theta$ ) in radians versus time ( $t$ ) in seconds, height 2 (0.16 m)

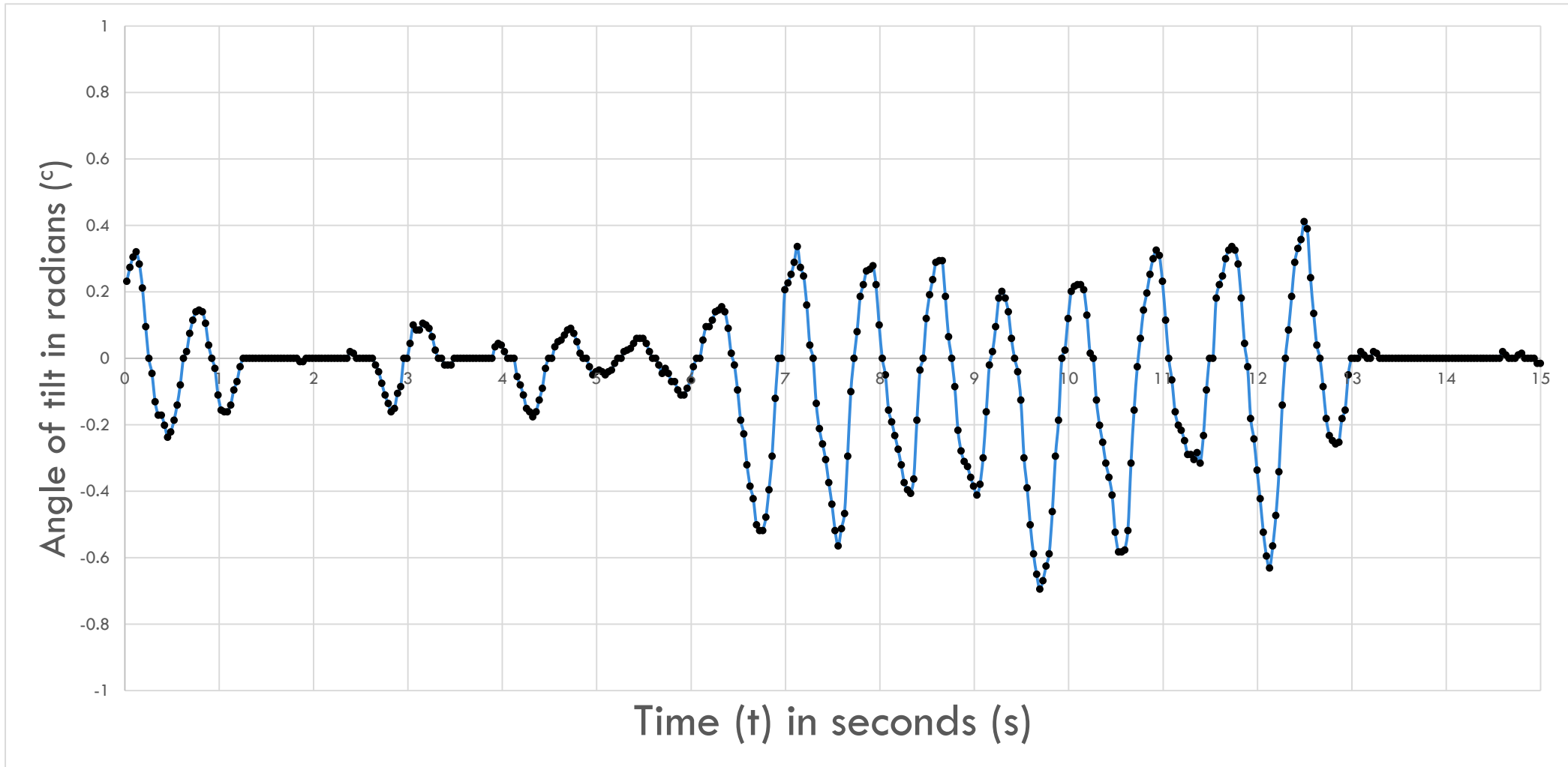


# SECOND DERIVATIVE (ANGULAR ACCELERATION)

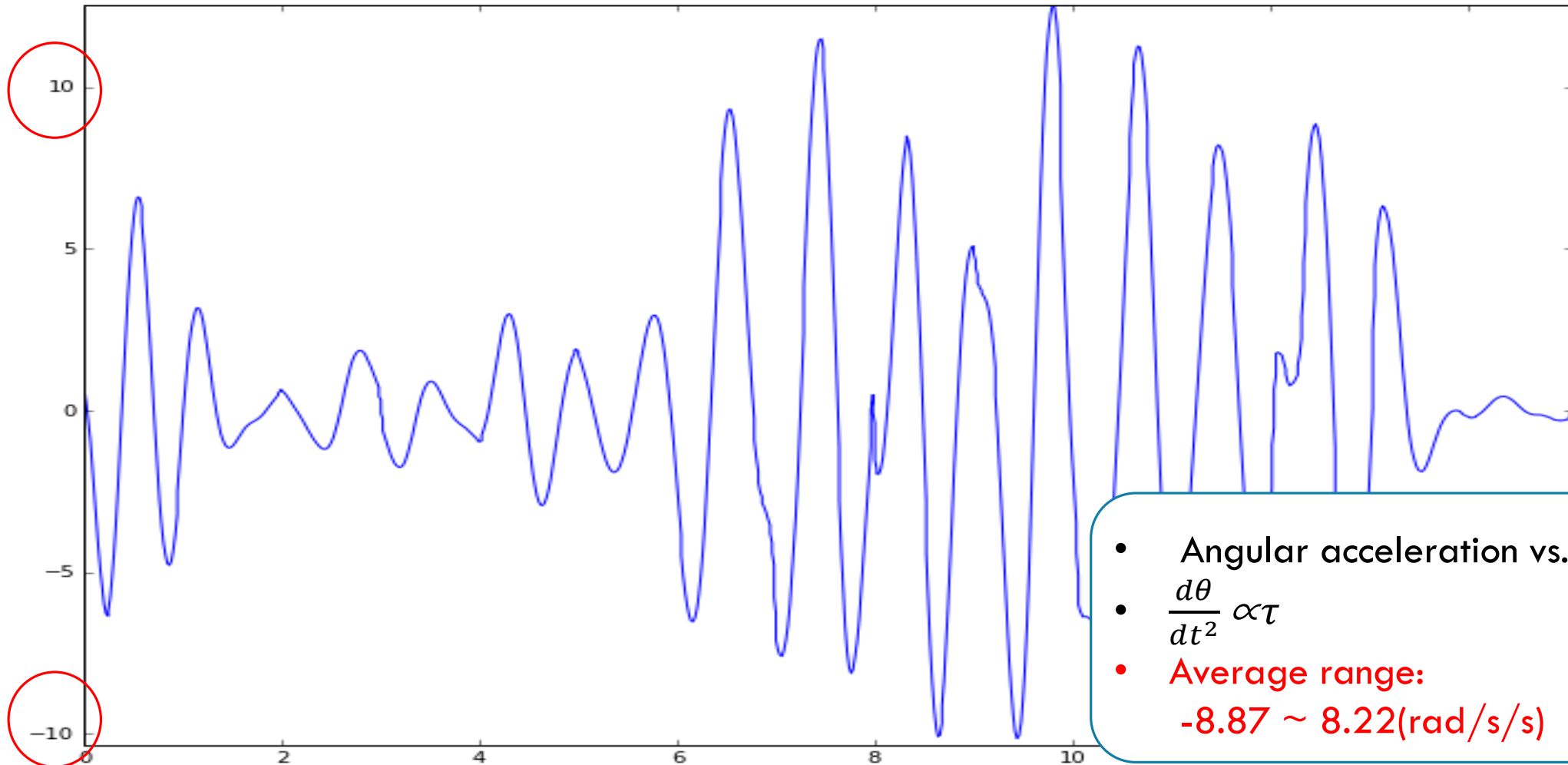


- Angular acceleration vs. time
- $\frac{d\theta}{dt^2} \propto \tau$
- Average range:  
-2.49 ~ 3.63(rad/s/s)

# RESULT 3: **0.24M** EFFECTIVE HEIGHT OF CM

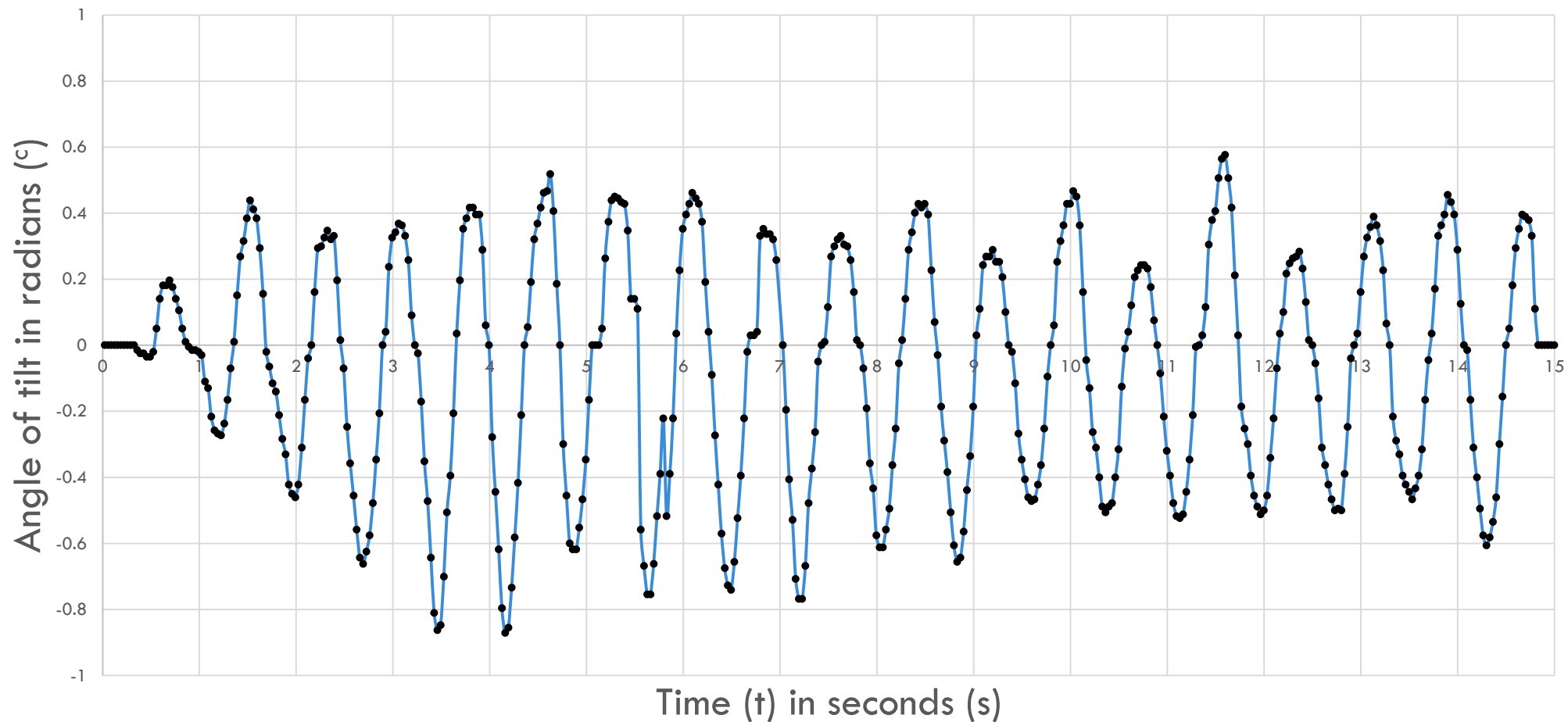


# SECOND DERIVATIVE (ANGULAR ACCELERATION)

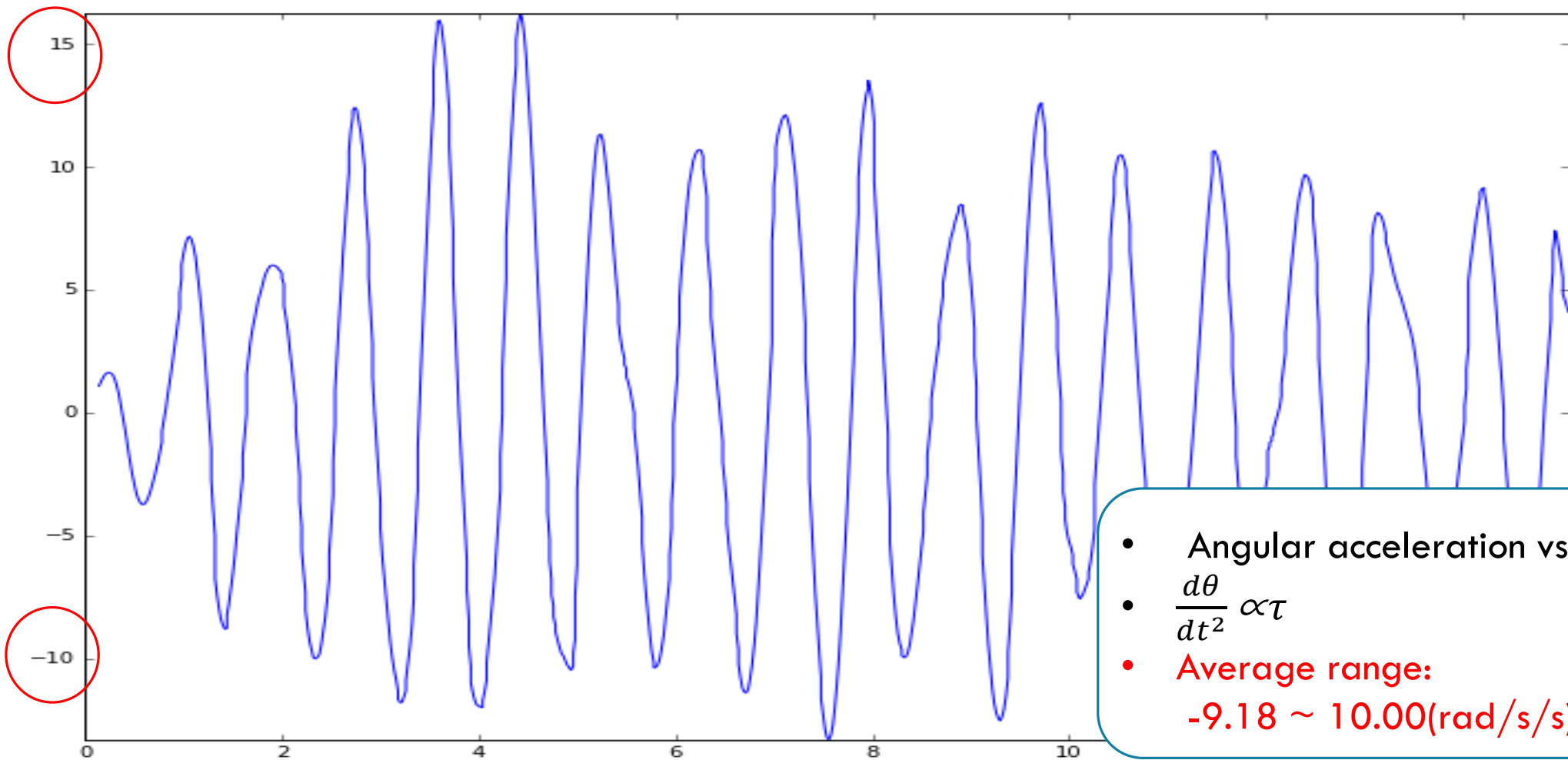


- Angular acceleration vs. time
- $\frac{d\theta}{dt^2} \propto \tau$
- Average range:  
-8.87 ~ 8.22(rad/s/s)

## RESULT 4: **0.32M** EFFECTIVE HEIGHT OF CM



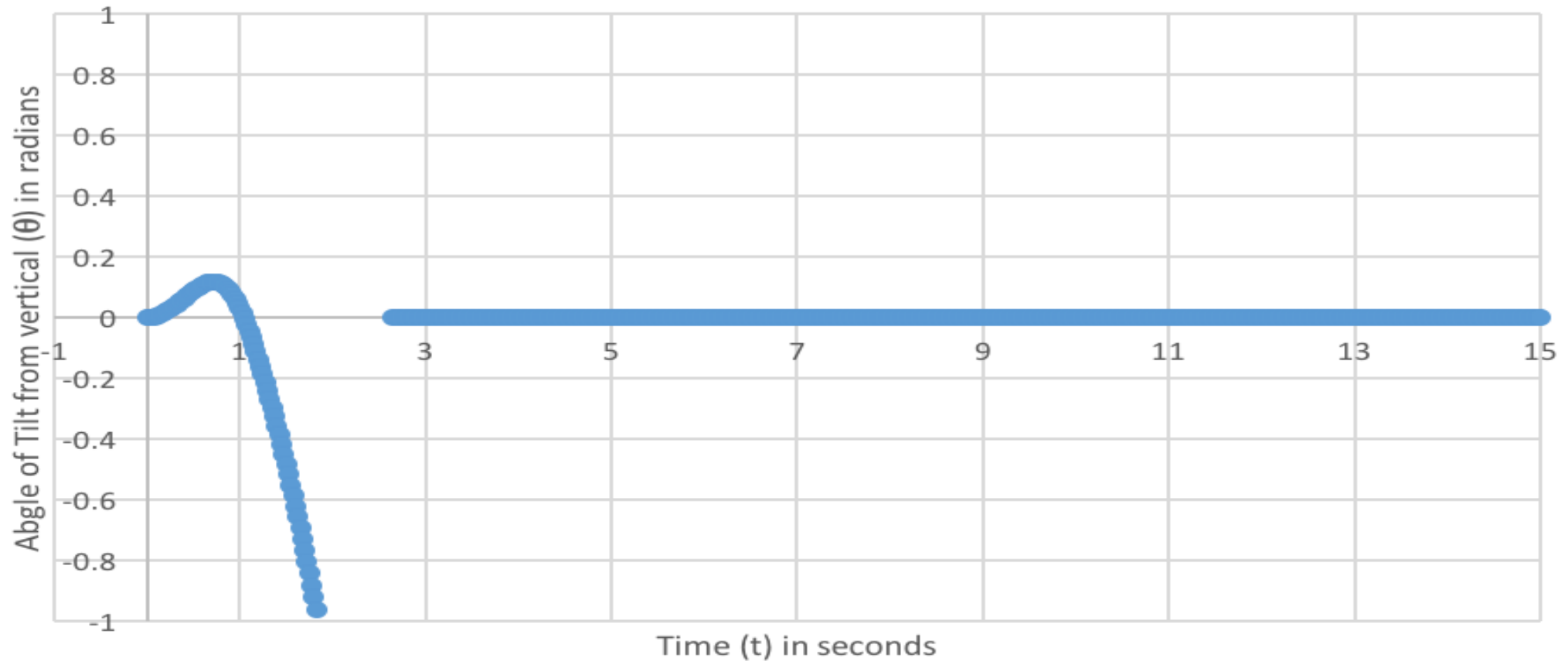
# SECOND DERIVATIVE (ANGULAR ACCELERATION)



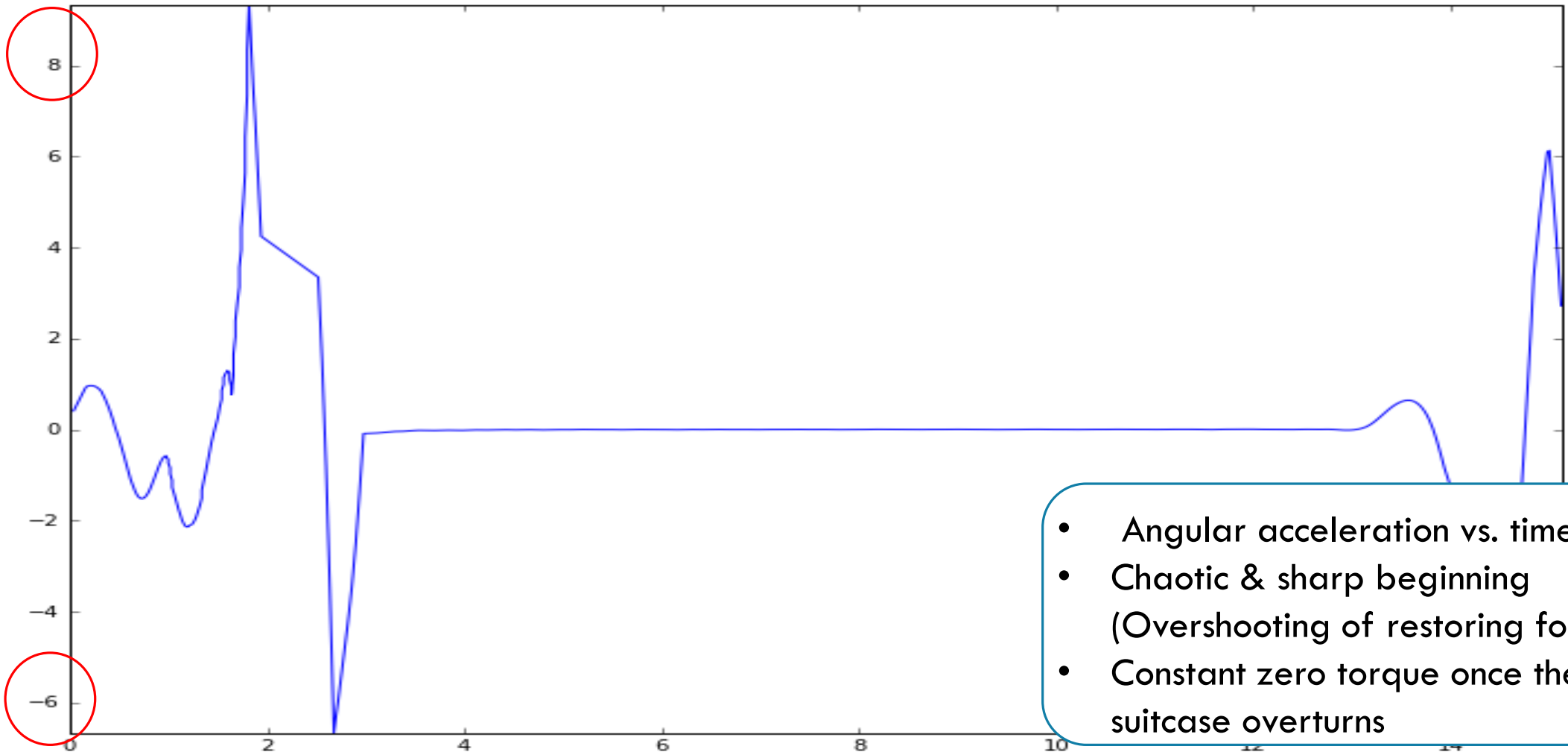
- Angular acceleration vs. time
- $\frac{d\theta}{dt^2} \propto \tau$
- Average range:  
-9.18 ~ 10.00(rad/s/s)



## RESULT 5: 0.40M EFFECTIVE HEIGHT OF CM (OVERTURN)




# SECOND DERIVATIVE (ANGULAR ACCELERATION)



- Angular acceleration vs. time
- Chaotic & sharp beginning (Overshooting of restoring force)
- Constant zero torque once the suitcase overturns

# SUMMARY OF EXPERIMENTAL RESULT (SET A)

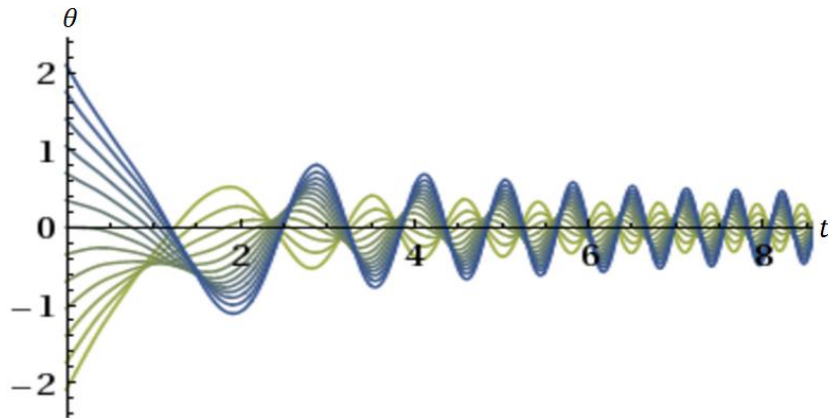
| Effective Height (m) | Range of angular acceleration (rad/s/s) | Average angular acceleration (rad/s/s) |
|----------------------|---|--|
| 0.08                 | -1.02 ~ 0.88                            | 0.95                                   |
| 0.16                 | -2.49 ~ 3.63                            | 3.06                                   |
| 0.24                 | -8.87 ~ 8.22                            | 8.54                                   |
| 0.32                 | -9.18 ~ 10.00                           | 9.59                                   |
| 0.40                 | Overturn                                | N/A                                    |



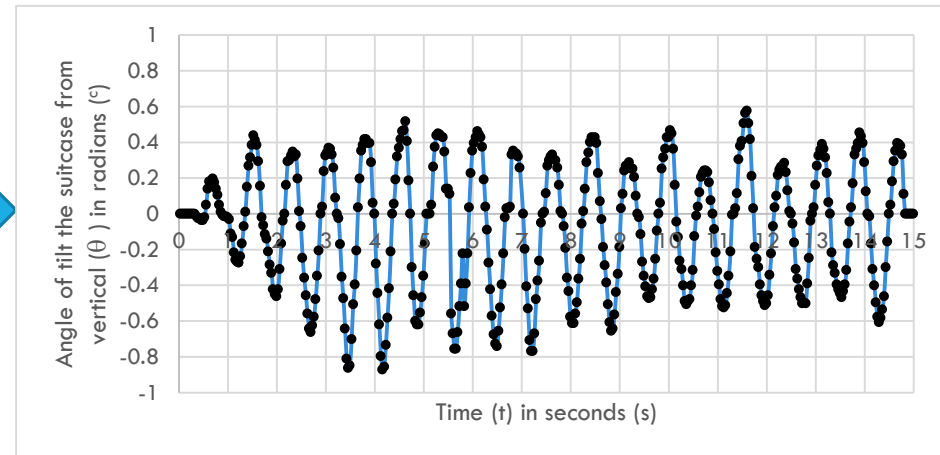
**As effective height increases:**  
= Increase in angular acceleration  
= Increase in torque  
= Increase in wobble  
= MORE LIKELY TO OVERTURN

# COMPARISON TO THEORETICAL PREDICTION

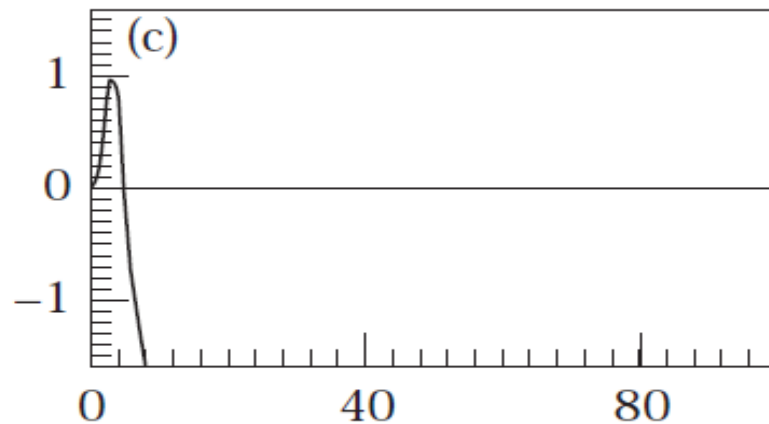
**Theory (Oscillation)**



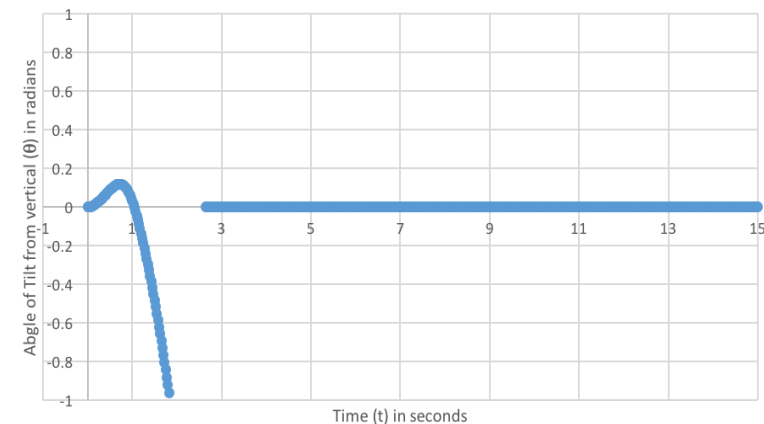
**Experiment (Oscillation)**



**Theory (Overturn)**

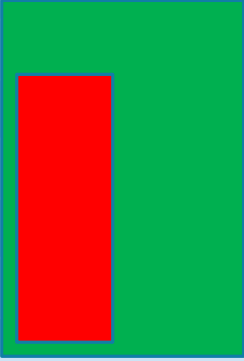


**Experiment (Overturn)**



Verified!

# SUMMARY OF EXPERIMENTAL RESULT (SET B)

| Weight Dist.  | Speed (m/s) | Angle | Wobbles | Overturn | Weight Dist.     | Speed (m/s) | Angle | Wobbles | Overturn |
|---|-------------|-------|---------|----------|------------------|-------------|-------|---------|----------|
| Pivot wheel   | ""          | 70°   | 1       | 1        | Obstructed wheel | ""          | 70°   | 0       | 0        |
|  |             |       | 1       | 1        |                  |             |       | 0       | 0        |
|   |             |       | 1       | 1        |                  |             |       | 0       | 0        |
|   |             |       | 1       | 1        |                  |             |       | 0       | 0        |
|   |             | 60°   | 1       | 1        |                  |             | 60°   | 0       | 0        |
|   |             |       | 1       | 1        |                  |             |       | 0       | 0        |
|   |             |       | 1       | 1        |                  |             |       | 0       | 0        |
|   |             | 50°   | 5       | 0        |                  |             | 50°   | 0       | 0        |
|   |             |       | 2       | 1        |                  |             |       | 0       | 0        |
|   |             |       | 1       | 1        |                  |             |       | 0       | 0        |
|   |             | 40°   | 1       | 1        |                  |             |       | 0       | 0        |
|   |             |       | 1       | 1        |                  |             |       |         |          |
|   |             |       | 1       | 1        |                  |             |       |         |          |

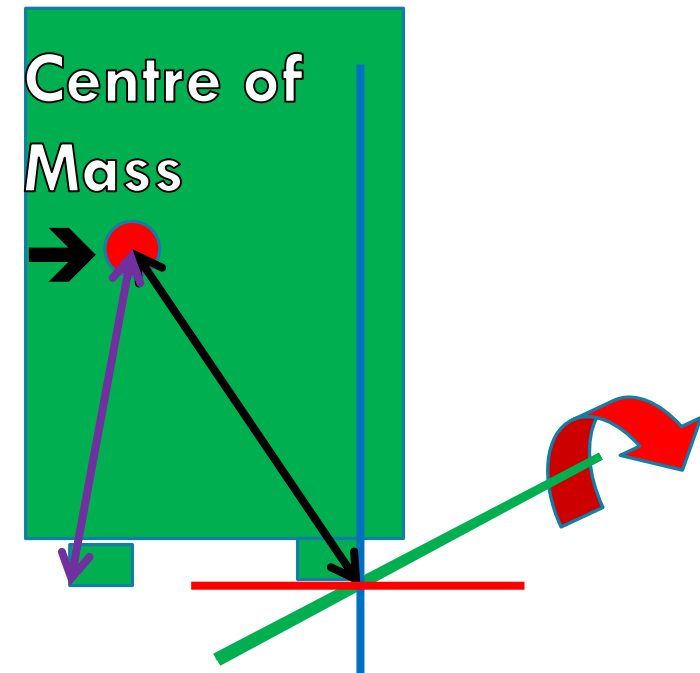
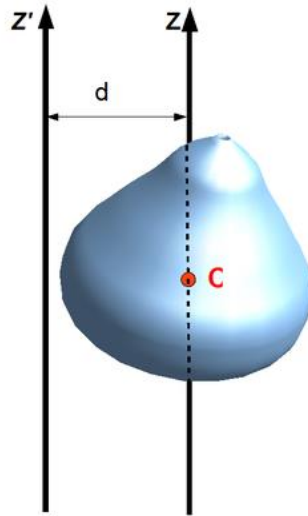
Potential outlier @ 50° for opposite wheel

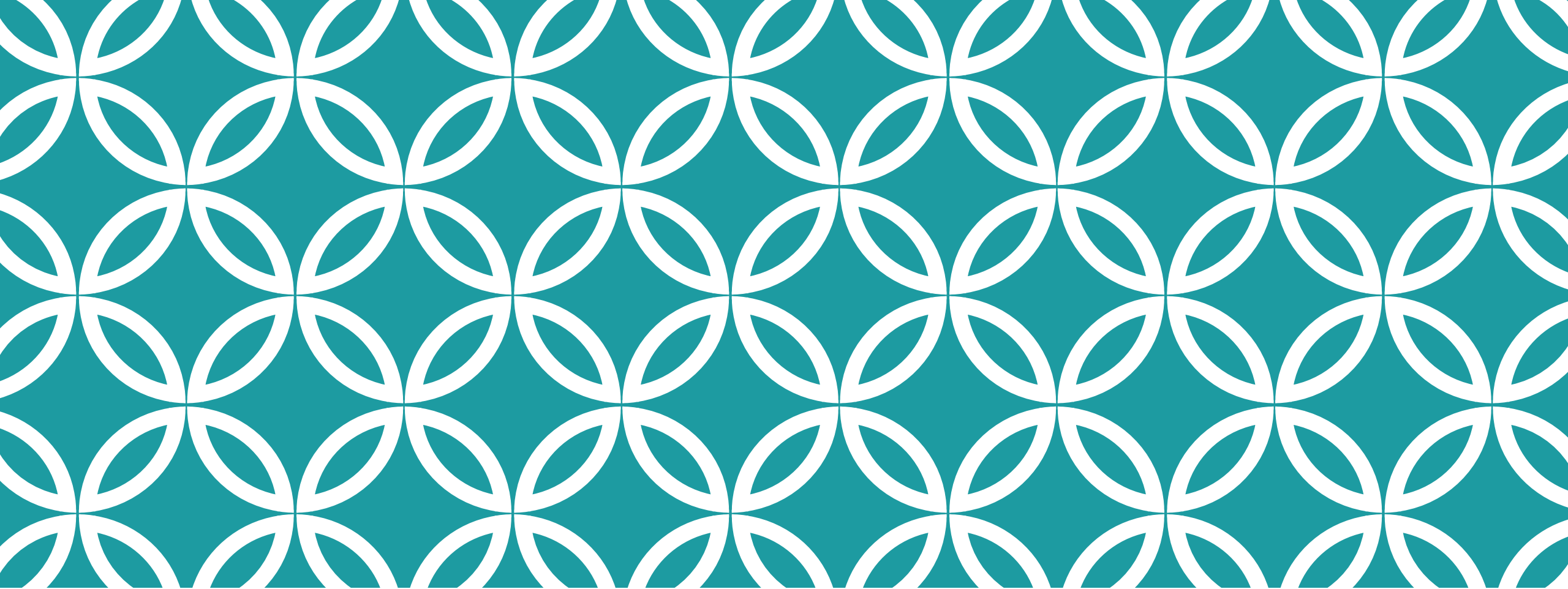
# RESULTS DISCUSSION (SET B)

The **closer the centre of mass** to the **obstructed wheel** the **less wobbles/overturns** the suitcase will have (Parallel axis Theorem).

Having the **centre of mass closer to the pivot wheel** causes **more instability**.

$$I = I_{CM} + md^2$$





# FURTHER CIRCUMSTANCES OF OVERTURN

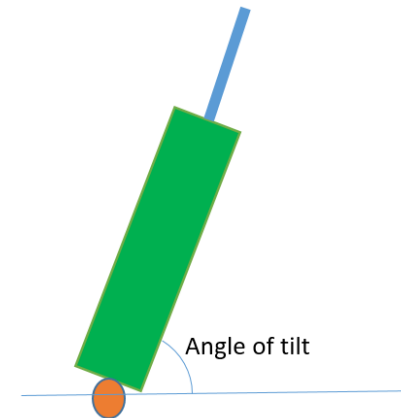
- Walking speed
- Angle of tilt
- Mass density
- Coefficient of Restitution

## 1) Angle of tilt vs Walking speed

| Degree of tilt | 0.81 m/s | 0.92 m/s | 1.04 m/s |
|----------------|----------|----------|----------|
| 70°            | O        | O        | O        |
| 60°            | N        | O        | O        |
| 50°            | N        | O        | O        |
| 40°            | N        | N        | N        |



APP FOR WALKING SPEED



ANGLE OF TILT

At 0.81 m/s, stable until high angles.  
At 1.04 m/s, stability reduced (high variations in  $\tau_H$ )



## 2) LOW WEIGHT:

### Mass density vs Walking speed

| No added mass | 0.92 m/s |
|---------------|----------|
| 70°           | O        |
| 60°           | O        |
| 50°           | N        |
| 40°           | N        |
| 1.5 kg mass   | 0.92 m/s |
| 70°           | O        |
| 60°           | O        |
| 50°           | N        |
| 40°           | N        |
| 3 kg mass     | 0.92 m/s |
| 70°           | O        |
| 60°           | N        |
| 50°           | N        |
| 40°           | N        |
| 30°           | N        |

## 3) HIGH WEIGHT:

### Mass density vs Walking speed

| No added mass | 0.92 m/s |
|---------------|----------|
| 70°           | O        |
| 60°           | O        |
| 50°           | O        |
| 40°           | N        |
| 1.5 kg mass   | 0.92 m/s |
| 70°           | O        |
| 60°           | N        |
| 50°           | N        |
| 40°           | N        |
| 3 kg mass     | 0.92 m/s |
| 70°           | N        |
| 60°           | N        |
| 50°           | N        |
| 40°           | N        |
| 30°           | N        |

For low weight:  
As mass is  
increased, stability  
increases.

$\tau_w \downarrow$

For high weight:  
As mass is  
increased, stability  
decreases.

$\tau_w \uparrow$

#### 4) COR vs Walking speed

| Indoor<br>(COR 0.35) | 0.81 m/s | 0.92 m/s | 1.04 m/s | Outdoor<br>(COR 0.68) | 0.81 m/s | 0.92 m/s | 1.04 m/s |
|----------------------|----------|----------|----------|-----------------------|----------|----------|----------|
| 70°                  | O        | O        | O        | 70°                   | O        | O        | O        |
| 60°                  | N        | O        | O        | 60°                   | O        | O        | O        |
| 50°                  | N        | O        | O        | 50°                   | O        | O        | O        |
| 40°                  | N        | N        | N        | 40°                   | O        | -        | -        |

- At lower walking frequency, suitcase was **less stable for trials outdoors**, due to **higher COR** and less energy loss.
- At **higher walking frequency**, energy loss is less significant due to **balancing effect of higher walking frequency**.

# CONCLUSION

Investigated circumstances when suitcase wobbles and turns over.

1. Developed mathematical simulation to model the wobble (FFT)
2. Simulation verified -> Comparison to theory
3. Studied effect of varied packing of the luggage
  - A. Significance of effective height of CM
  - B. Effect of other positions of CM vs. Wheel Position
4. Considered other factors that influence the wobble
  - A. Walking Frequency
  - B. Angle of tilt
  - C. Coefficient of Restitution
  - D. Different mass density

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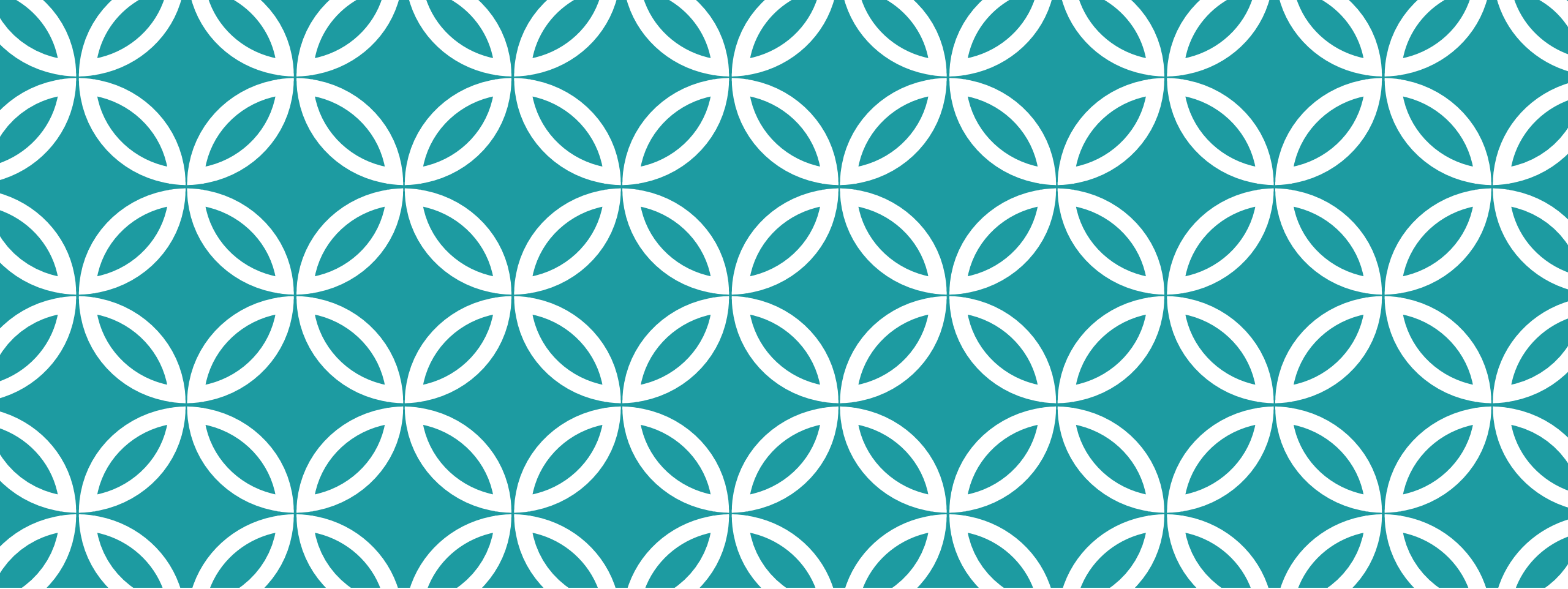


# ACKNOWLEDGEMENT

Thanks for your time

Mr Richard Jones

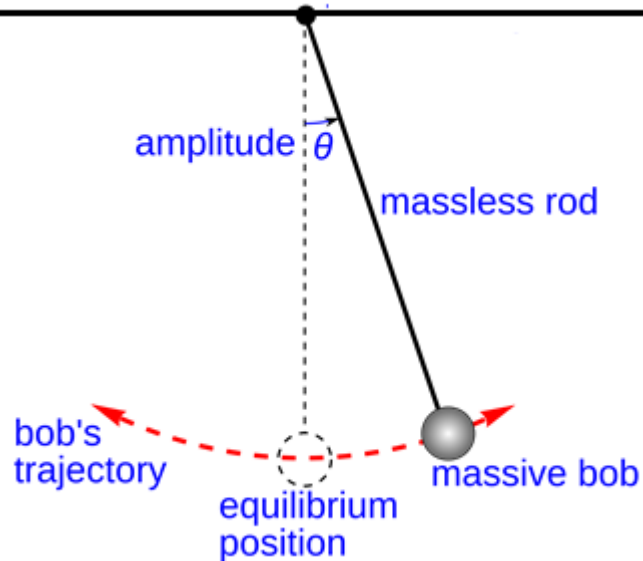
Finn Connolly



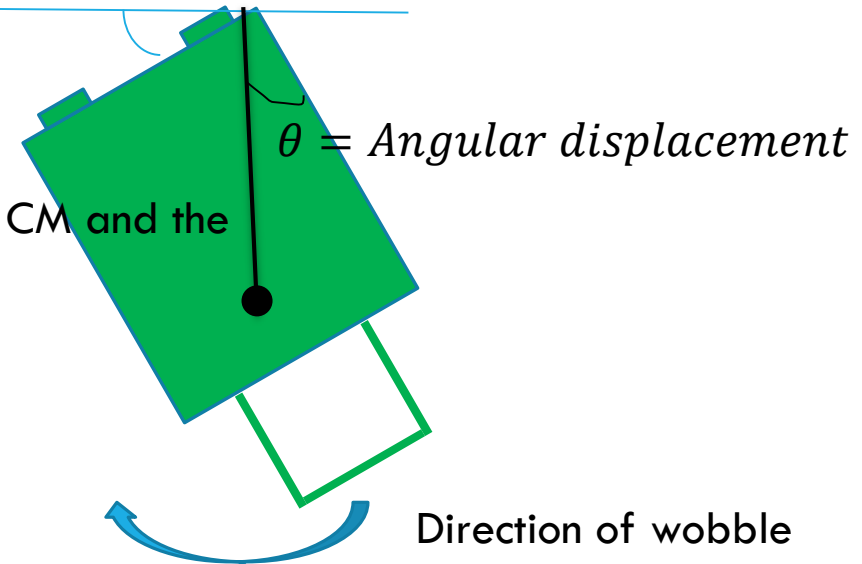
**THANK YOU!**

Team of Australia  
Reporter: Jeong Han Song

# SUITCASE AS AN “INVERTED PENDULUM”

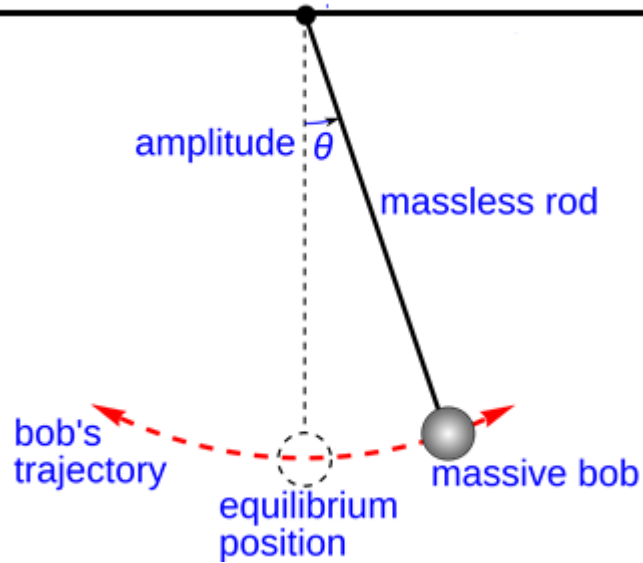


Distance between CM and the Pivot point



| Simple Pendulum    | Crazy Suitcase                    |
|--------------------|-----------------------------------|
| Massive Bob        | Centre of mass of packing         |
| Amplitude $\theta$ | Angular Displacement $\theta$     |
| Length of Rod      | Distance between CM and the Pivot |
| Bob's trajectory   | Direction of wobble               |

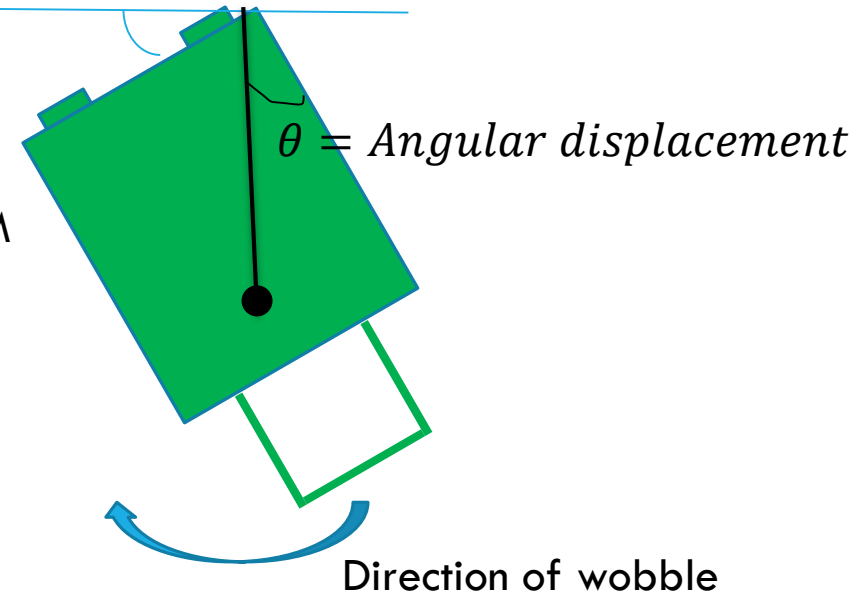
# SUITCASE AS AN “INVERTED PENDULUM”



Distance between CM  
and the Pivot point

$$f = \frac{1}{2\pi} \sqrt{\frac{g}{l}}$$

Length of Rod



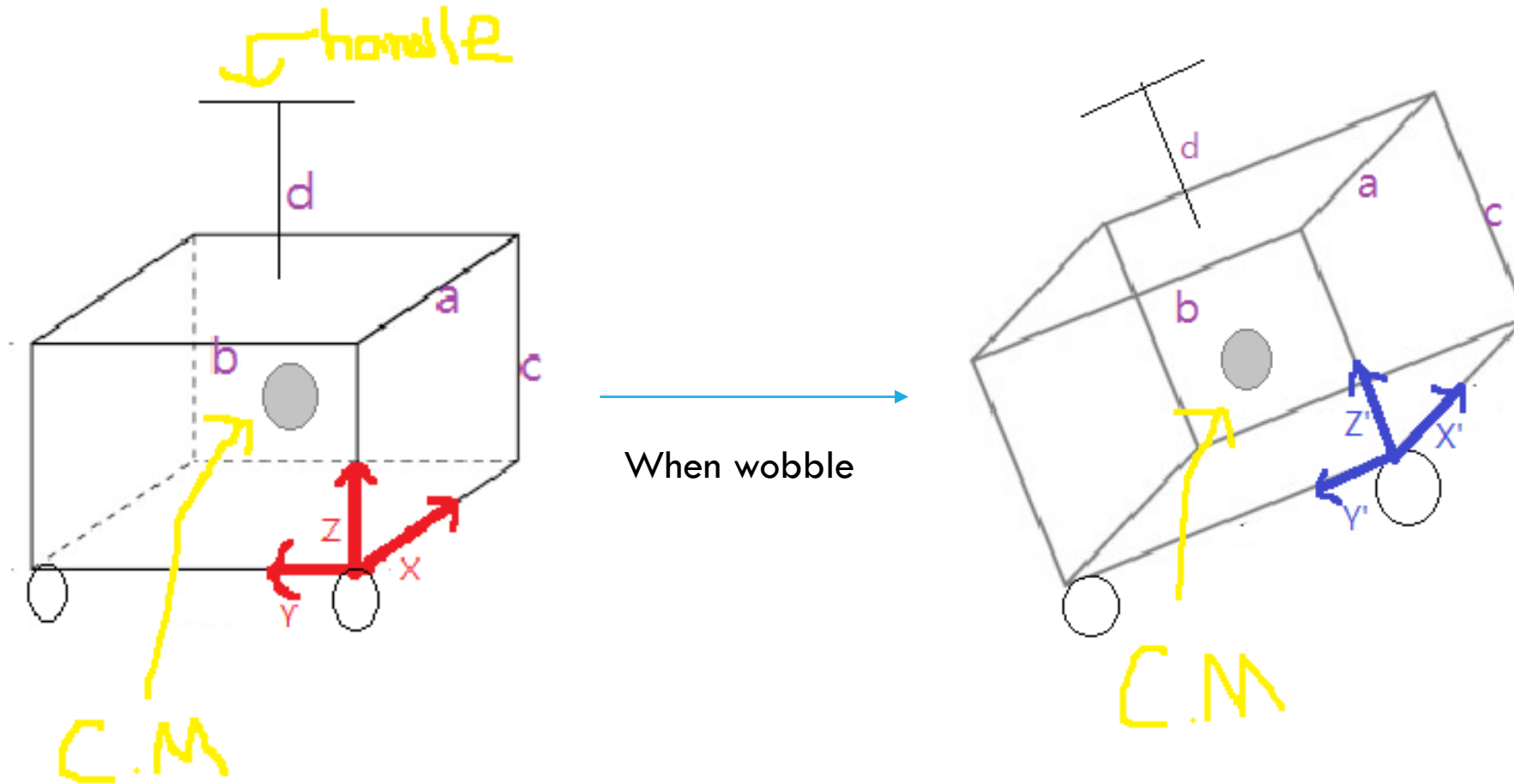
Relation between effective height  
and the frequency of oscillation



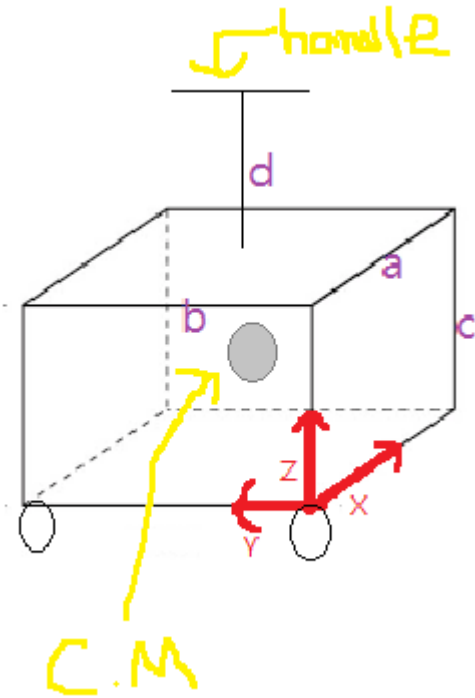
# ASSUMPTIONS

1. A constant initial disturbance was employed to start the wobble (e.g. instability) of a suitcase.
2. The suitcase and its wheels were regarded as rigid bodies.
3. Human always responded to the instability by exerting restoring torques that were ***just enough*** to stabilise the motion
4. Human response time was always constant

# SUITCASE IN 3-DIMENSION



# SUITCASE IN 3-DIMENSION

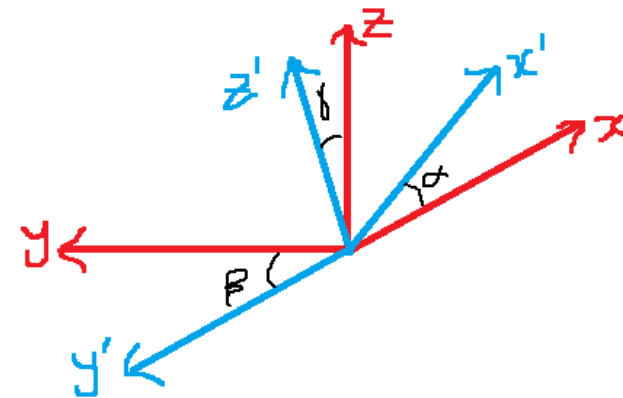
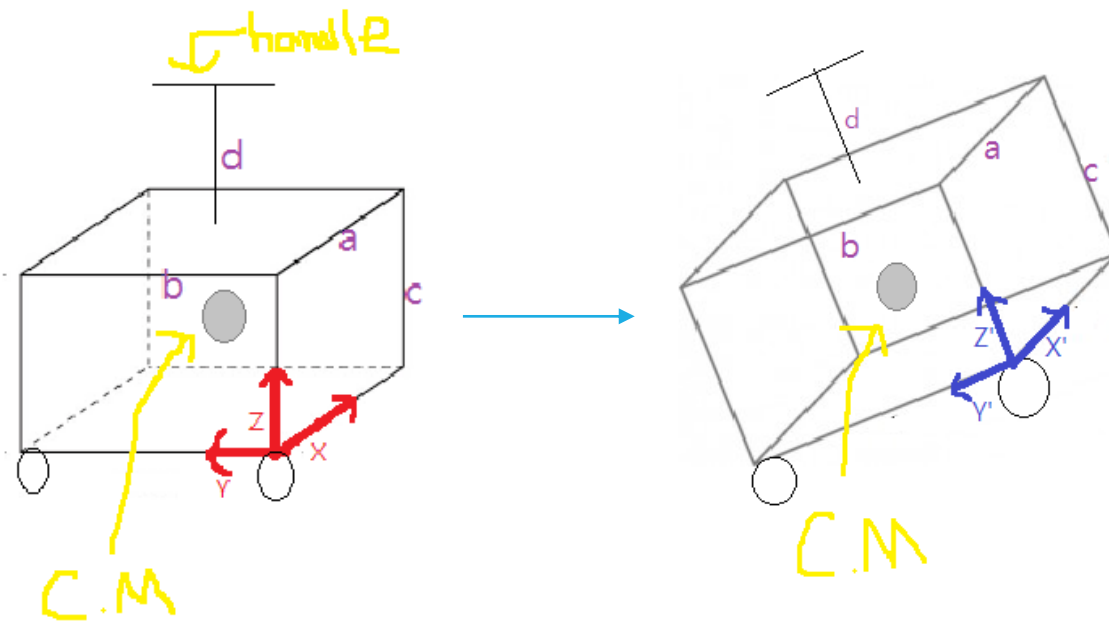


$$CM \rightarrow \left( \frac{a}{2}, \frac{b}{2}, c \right) = (x, y, z)$$

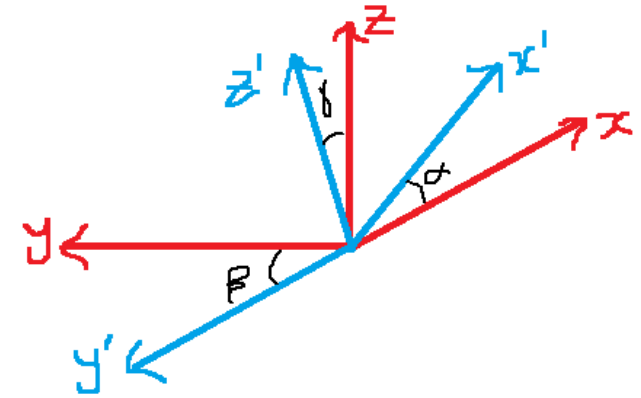
$$\text{Handle} \rightarrow \left( \frac{a}{2}, \frac{b}{2}, c + d \right) = (X, Y, Z)$$

# SUITCASE IN 3-DIMENSION

Change in co-ordinate when tilted



# SUITCASE IN 3-DIMENSION

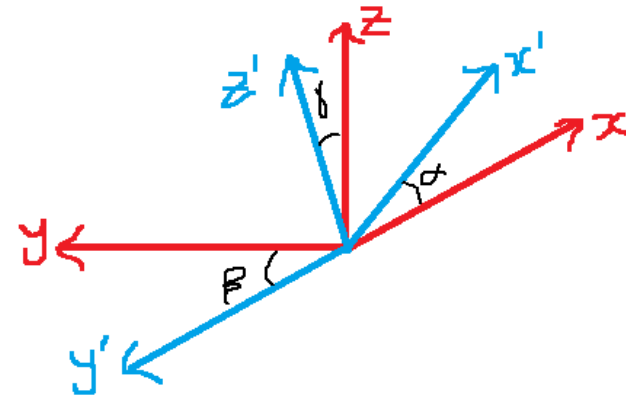


When a suitcase is initially pulled by a person, there will be a rotation about  $y$ -axis.

This rotation is followed by  $x$ -axis and  $z$ -axis.

# POSSIBLE WOBBLING MOTI

## - GENERAL FORMULA



$$\begin{pmatrix} x' \\ y' \\ z' \end{pmatrix} = \begin{pmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \beta & \sin \beta \\ 0 & -\sin \beta & \cos \beta \end{pmatrix} \begin{pmatrix} \cos \gamma & 0 & \sin \gamma \\ 0 & 1 & 0 \\ -\sin \gamma & 0 & \cos \gamma \end{pmatrix} \begin{pmatrix} \frac{a}{2} \\ \frac{b}{2} \\ c \end{pmatrix}$$

NEW  
Centre of  
Mass

z-axis

x-axis

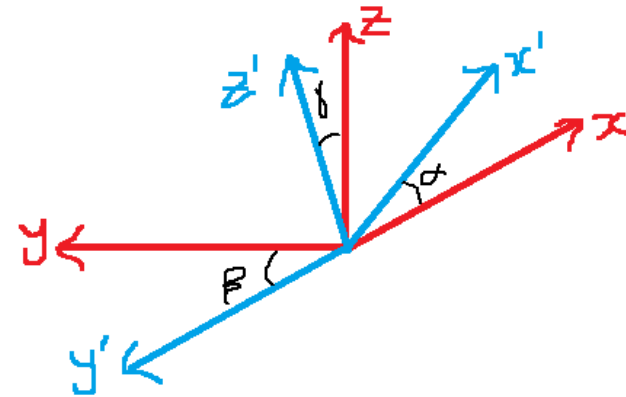
y-axis

PREVIOUS  
Centre of  
Mass

**SHIFT IN CENTRE OF MASS OF AN OBJECT**

# POSSIBLE WOBBLING MOTI

## - GENERAL FORMULA



$$\begin{pmatrix} X' \\ Y' \\ Z' \end{pmatrix} = \begin{pmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \beta & \sin \beta \\ 0 & -\sin \beta & \cos \beta \end{pmatrix} \begin{pmatrix} \cos \gamma & 0 & \sin \gamma \\ 0 & 1 & 0 \\ -\sin \gamma & 0 & \cos \gamma \end{pmatrix} \begin{pmatrix} \frac{a}{2} \\ \frac{b}{2} \\ d + z \end{pmatrix}$$



NEW  
Centre of  
Mass



z-axis



x-axis



y-axis



PREVIOUS  
Centre of  
Mass

**SHIFT IN CENTRE OF MASS OF A HANDLE**

# POSSIBLE WOBBLING MOTIONS

## - GENERAL FORMULA

$$\begin{aligned}
 R_z R_x R_y &= \begin{pmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \beta & \sin \beta \\ 0 & -\sin \beta & \cos \beta \end{pmatrix} \begin{pmatrix} \cos \gamma & 0 & \sin \gamma \\ 0 & 1 & 0 \\ -\sin \gamma & 0 & \cos \gamma \end{pmatrix} \\
 &= \begin{pmatrix} \cos \alpha & \sin \alpha \cos \beta & \sin \alpha \sin \beta \\ -\sin \alpha & \cos \alpha \cos \beta & \cos \alpha \sin \beta \\ 0 & -\sin \beta & \cos \beta \end{pmatrix} \begin{pmatrix} \cos \gamma & 0 & \sin \gamma \\ 0 & 1 & 0 \\ -\sin \gamma & 0 & \cos \gamma \end{pmatrix} \\
 &= \begin{pmatrix} \cos \alpha \cos \gamma - \sin \alpha \sin \beta \sin \gamma & \sin \alpha \cos \beta & \cos \alpha \sin \gamma + \sin \alpha \sin \beta \cos \gamma \\ -\cos \alpha \sin \beta \sin \gamma - \sin \alpha \cos \gamma & \cos \alpha \cos \beta & \cos \alpha \sin \beta \sin \gamma - \sin \alpha \sin \gamma \\ -\cos \beta \sin \gamma & -\sin \beta & \cos \beta \cos \gamma \end{pmatrix}
 \end{aligned}$$